

INSPECTION REPORT
Sedimentation Structure
N10-B1
Kayenta Mine
Navajo County, Arizona
for
PEABODY COAL COMPANY



Dames & Moore
10139-011-22

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INTRODUCTION

Sedimentation Structure N10-B1 is an earthen embankment, designed and constructed in 1981 by Peabody Coal Company as a temporary sedimentation structure to control runoff and sediment from the disturbed mining areas of the Kayenta Mine. The location of Structure N10-B1 is shown on Plate 1, Site Plan.

This inspection report contains information specific to Structure N10-B1. Regional site information is presented in the "General Report, Kayenta and Black Mesa Mines, Navajo County, Arizona for Peabody Coal Company," along with the methods and results of analyses used for slope stability, hydrology and hydraulics.

INSPECTION

Structure N10-B1 was inspected on September 9, 1985 by an interdisciplinary team of engineers from Dames & Moore. The purpose of the inspection was to assess the safety and general condition of the structure with respect to United States Department of Interior, Office of Surface Mining (OSM) regulations.

Dames & Moore's inspection was performed in accordance with applicable 30 CFR 780 and 816 regulations and included a review of the N10-B1 project files and a field inspection of the structure. The most current information contained in the Peabody Coal Company files includes the 1984 and current survey data and inspections performed in 1984 and 1985 by

Peabody Coal Company. The survey data developed in August 1984 was used in the analyses of the structure. Results of the field inspection are included in this report as Appendix A.

SITE DESCRIPTION

LAND USE

Structure N10-B1 has a 10.6-acre tributary drainage area and is located near Coal Mine Wash at the Kayenta Mine. The watershed is classified as 51% reclaimed and 49% Pinion/Juniper.

EMBANKMENT

Structure N10-B1 is a homogeneous earthen embankment classified as a sidehill embankment. Physical characteristics of the embankment are listed in the following table:

Structure N10-B1

Embankment	Residual Sandstone Soils
Foundation	Residual Sandstone Soils
Right Abutment	Fill
Left Abutment	Residual Sandstone Soils
Height	9.4 ft
Crest Width	12 ft
Upstream Slope	1.9 H : 1 V
Downstream Slope	2.9 H : 1 V

A cross-section of the embankment is shown on Plate 2, Existing Maximum Cross Section N10-B1, A-A'.

ANALYSES

STABILITY

Structure N10-B1 is a category A-1 embankment. A standard category A-1 embankment has static and seismic factors of safety of 1.5 and 1.2, respectively, under the following conditions:

1. Maximum height = 15 ft
2. Maximum upstream slope = 1.75 H : 1 V
3. Maximum downstream slope = 3.25 H : 1 V
4. Normal pool with steady seepage saturation conditions

The N10-B1 embankment is lower in height; however, the downstream slope is steeper than the category standard; therefore, the embankment has factors of safety less than the design minimum.

HYDROLOGY

The hydrologic analysis was completed using the U.S. Army Corps of Engineers generalized computer program HEC-1, Flood Hydrograph Package. Structure N10-B1 is not in series with any other structure and therefore the spillway was analyzed using the 25-year, 6-hour storm. The storage capacity of Structure N10-B1 was analyzed using the 10-year, 24-hour storm.

The following parameters were used in the hydrologic analysis:

1. Water Course length, L	0.379	mi
2. Elevation Difference, H	130	ft
3. Time of Concentration, T	0.130	h
4. Lag time, $0.6T_c$	0.078	h
5. SCS Curve Number	82	
6. Rainfall Depth, 10-year, 24-hour storm .	2.1	in.
25-year, 6-hour storm. .	1.9	in.
7. Drainage Area	10.6	acres

HYDRAULICS

The HEC-1 program was used to evaluate inflow to the sedimentation structure, outflow from the structure and the resulting water surface elevations. The initial conditions and results of the analysis are summarized in the following table.

N10-B1 HYDRAULICS

	Units	10-year 24-hour Storm	25-year 6-hour Storm
<hr/>			
Initial Reservoir Volume			
Condition		Empty	Full to the spillway elevation
Inflow			
Peak Flow	cfs	13	17
Volume	acre-ft	0.71	0.56
Storage			
Peak Stage	ft	6582.00	6588.74
Spillway Elevation . .	ft	6588.24	—
Peak Storage	acre-ft	0.71	—
Storage Capacity . . .	acre-ft	3.42	—
Outflow			
Peak Flow	cfs	0	3
Embankment Crest			
Elevation	ft	—	6590.13
Peak Stage	ft	—	6588.74
Freeboard	ft	—	1.39
Spillway Channel			
Flow Depth	ft	—	0.50
Critical Velocity. . .	fps	—	1.8
Manning's "n"		—	0.035
Outflow Channel			
			<u>Section I</u> <u>Section II</u>
Slope	%	—	35 14
Normal Velocity. . . .	fps	—	3.6 2.7
Normal Depth	ft	—	0.05 0.07
Manning's "n"		—	0.035 0.035

Spillway Channel

The existing spillway for N10-B1 has a trapezoidal channel with the following dimensions:

Channel depth	2.75	ft
Channel width	16	ft
Channel length	30	ft
Side slopes (horizontal to vertical). .	2:1	
Average exit slope	3	percent

Rock provides erosion protection within the channel.

Outflow Channel

The structure presently has no outflow channel.

STORAGE CAPACITY

The impoundment volume-elevation curve is based on site specific surveys conducted for Peabody Coal Company's August 1984 inspection, and 1985 resurveys, where available. Additionally, the most current topographic maps available were used in developing Plate 3, Volume-Elevation Curve, N10-B1.

The calculations for the sediment load entering Structure N10-B1 were made utilizing the Universal Soil Loss Equation with the following parameters:

1. Rainfall Factor, R 40
2. Soil Erodibility Factor, K 0.32
3. Slope Factor, LS 7.8
4. Cover Factor, C 0.145
5. Erosion Control Factor, P 1.0

The hydrologic analysis gives the storage volume required to contain the 10-year, 24-hour storm, and the remaining storage volume available for storing sediment. The existing storage capacity of N10-B1 and the results of the sediment inflow analysis are summarized in the following table.

N10-B1 STORAGE

Total Storage Capacity	3.42	acre-ft
10-year, 24-hour Storm Inflow	0.71	acre-ft
Available Sediment Storage Capacity	2.71	acre-ft
Sediment Inflow Rate	0.072	acre-ft/yr
Sediment Storage Life	38	yrs

REMEDIAL COMPLIANCE PLAN

GEOTECHNICS

The inspection of Structure N10-B1 indicated that the only geotechnical problem is rill erosion on the upstream and downstream slopes. Correction of erosion is considered a periodic maintenance task and does not require remedial action. The downstream slope should be flattened to 3.25 horizontal to 1 vertical to meet stability requirements.

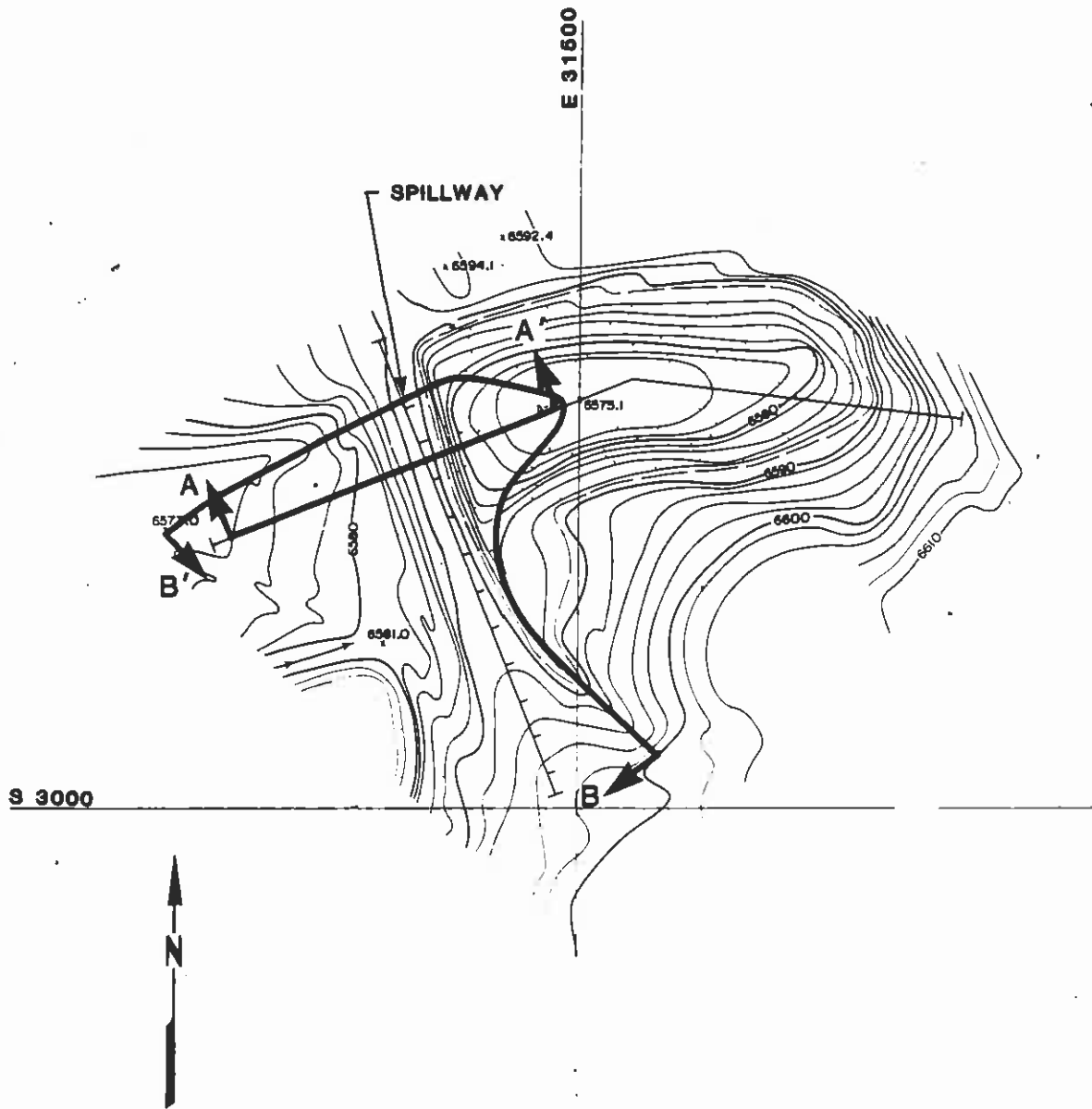
HYDRAULICS

The storage capacity and spillway capacity of Structure N10-B1 are adequate; however, the spillway does not have an adequate outflow channel. A trapezoidal outflow channel should be constructed along the alignment B-B' shown in Plate 1. The channel profile is shown in Plate 4 and the required dimensions are shown in Plate 5. The outflow channel should be protected against erosion using geotextile and gravel as shown in Plate 5.

* * *

The following plates and appendix are attached and complete this inspection report.

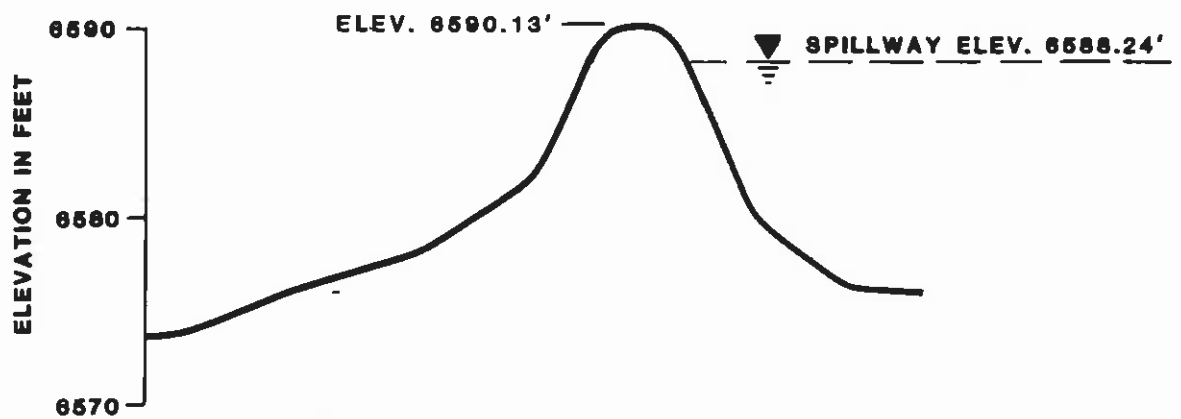
- Plate 1 - Site Plan N10-B1
- Plate 2 - Existing Maximum Cross Section N10-B1, A-A'
- Plate 3 - Volume-Elevation Curve N10-B1
- Plate 4 - Channel Profile N10-B1, B-B'
- Plate 5 - Spillway and Outflow Channel Cross Section N10-B1
- Appendix A - Inspection Check List
- Appendix B - Hydrology and Hydraulic Calculations



SITE PLAN N10-B1

BY **Dames & Moore**

Plate 1

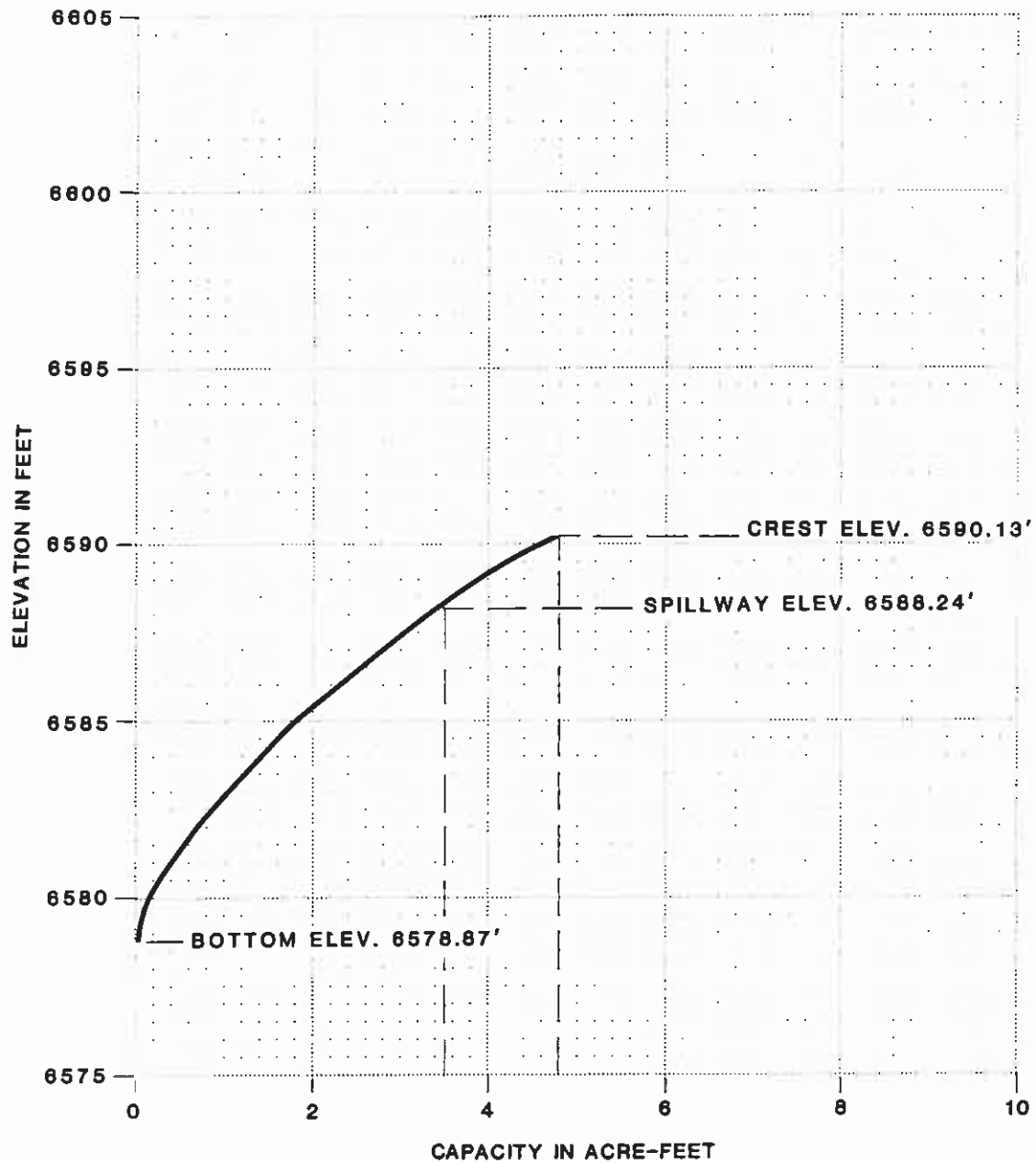


EXISTING
MAXIMUM CROSS-SECTION
A-A'
N10-B1

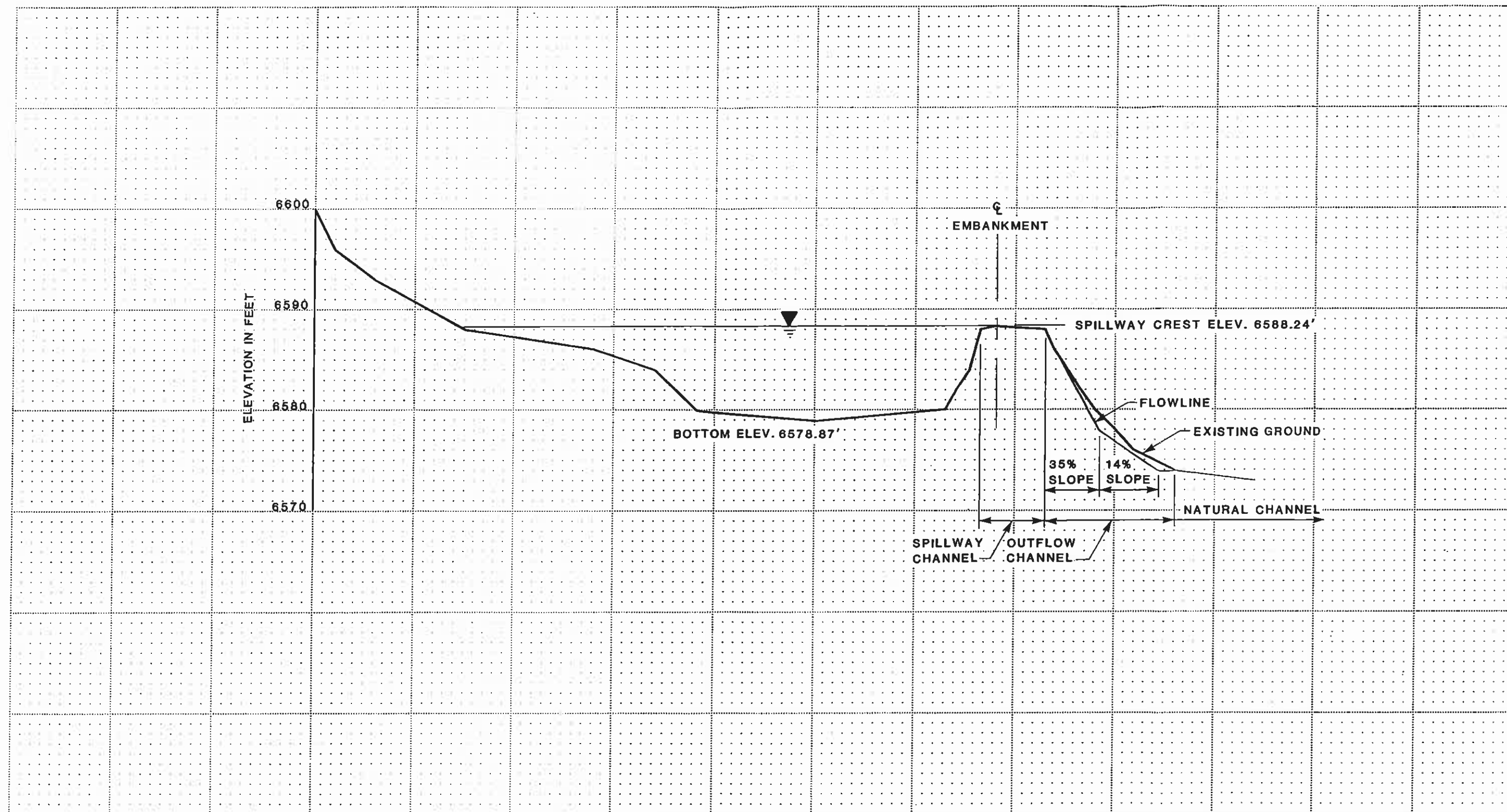
FOR LOCATION SEE PLATE 1

BY **Dames & Moore**

Plate 2

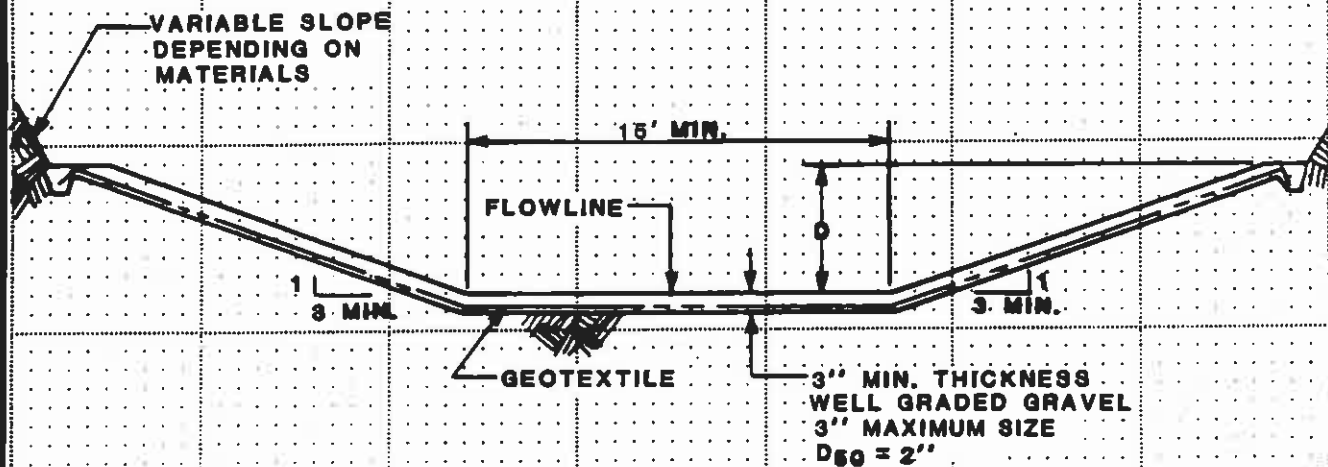


VOLUME-ELEVATION
CURVE
N10-B1



CHANNEL PROFILE B-B'
N10-B1





SPILLWAY CHANNEL

$D = 1.5'$
 LENGTH = 30'
 FLOWLINE ELEV. = 6588.24'

OUTFLOW CHANNEL

$D = 1'$

**SPILLWAY AND
 OUTFLOW CHANNEL
 CROSS SECTION
 N10-B1**

APPENDIX A
INSPECTION CHECK LIST

INSPECTION CHECK LIST

ITEM	YES	NO	REMARKS
1. CREST			12' w.
a. Any visual settlements?		X	
b. Misalignment?		X	
c. Cracking?		X	
2. UPSTREAM SLOPE			28°
a. Adequate grass cover?		X	
b. Any erosion?	X		Rills
c. Are trees growing on slope?		X	
d. Longitudinal cracks?		X	
e. Transverse cracks?		X	
f. Adequate riprap protection?		X	
g. Any stone deterioration?			NA
h. Visual depressions or bulges?		X	
i. Visual settlements?		X	
j. Animal burrows?		X	
3. DOWNSTREAM SLOPE			19°
a. Adequate grass cover?		X	
b. Any erosion?	X		Rills
c. Are trees growing on slope?		X	
d. Longitudinal cracks?		X	
e. Transverse cracks?		X	
f. Visual depressions or bulges?		X	
g. Visual settlements?		X	
h. Is the toe drain dry?			NA
i. Are the relief wells flowing?			NA
j. Are boils present at the toe?		X	
k. Is seepage present?		X	
l. Animal burrows?		X	
4. ABUTMENT CONTACT. RIGHT			
a. Any erosion?		X	
b. Visual differential movement?		X	
c. Any cracks noted?		X	
d. Is seepage present?		X	
e. Type of Material?			brown SM
5. ABUTMENT CONTACT. LEFT			
a. Any erosion?		X	
b. Visual differential movement?		X	
c. Any cracks noted?		X	
d. Is seepage present?		X	
e. Type of Material?			brown SM

ITEM	YES	NO	REMARKS
6. SPILLWAY/NORMAL			
a. Location:			
Left abutment?			
Right abutment?	X		
Crest of Embankments?			
b. Approach Channel:		X	
Are side slopes eroding?			NA
Are side slopes sloughing?			
Bottom of channel eroding?			
Obstructed?			
Erosion protection?			
c. Spillway Channel:			2.75' below crest 16' w. 30' L 3% S.
Are side slopes eroding?		X	
Are side slopes sloughing?		X	
Bottom of channel eroding?		X	
Obstructed?		X	
Erosion protection?	X		
d. Outflow Channel:		X	
Are side slopes eroding?			NA
Are side slopes sloughing?			
Bottom of channel eroding?			
Obstructed?			
Erosion protection?			
e. Weir:		X	
Condition?			
7. SPILLWAY/EMERGENCY			
a. Location:			NA
Left abutment?			
Right abutment?			
Crest of Embankments?			
b. Approach Channel:			
Are side slopes eroding?			
Are side slopes sloughing?			
Bottom of channel eroding?			
Obstructed?			
Erosion protection?			
c. Spillway Channel:			
Are side slopes eroding?			
Are side slopes sloughing?			
Bottom of channel eroding?			
Obstructed?			
Erosion protection?			
d. Outflow Channel:			
Are side slopes eroding?			
Are side slopes sloughing?			
Bottom of channel eroding?			
Obstructed?			
Erosion protection?			
e. Weir:			
Condition?			

ITEM	YES	NO	REMARKS
8. IMPOUNDMENT			
a. Sinkholes?		<input checked="" type="checkbox"/>	(Elev.) feet
b. Water present?		<input checked="" type="checkbox"/>	(Elev.) feet
c. Siltation?	<input checked="" type="checkbox"/>		
d. Watershed matches soil map?	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	

9. GENERAL COMMENTS

EROSION GULLEY OFF THE INCISED SLOPE,
INTO POND

24" cul enters from u.s. of LA - blocked completely
on upstream end.

Canopy 25
Ground 65

APPENDIX B

HYDROLOGY AND HYDRAULIC CALCULATIONS

TIME OF CONCENTRATION

ELEVATION DIFFERENCE = $6715 - 6585 = 130$ ft.

WATER COURSE LENGTH = $5.0(400) = 2000$ ft. = 0.379 mi.

$T_c = \left(\frac{11.9 (0.379)^3}{130} \right)^{0.385} = 0.130$ hr. \approx

Lag Time = $0.6 T_c = 0.078$ hr. \approx

SCS CURVE NUMBER

DRAINAGE AREA (ac)	COVER TYPE	HYDROLOGIC CONDITION	SOIL TYPE	WEIGHTED CURVE NUMBER
5.2	P-I	average	D	83 (.49)
5.4	not - and Retained	fair		81 (.51)
				<hr/> 81.98
				use <u>82</u>

50% # 25
 50% # 35

DRAINAGE BASIN AREA

10.6 ACRES

0.017 SQ MILES

REVISIONS

BY _____ DATE _____ TO EO _____
 BY _____ DATE _____ TO EO _____

BY S. DOLAN DATE 9-23-85
 CHECKED BY _____
 COPY TO EO _____

UNIVERSAL SOIL LOSS EQUATION

RAINFALL FACTOR

$$K = 4.7$$

SOIL ERODIBILITY FACTOR

SOIL TYPE =	50% reclaimed	.50(.42)
	50% #25	.5(.22)
		<u>.32</u>

$$K = \underline{\underline{.32}}$$

SLOPE FACTOR

LENGTH (ft.)	Δ ELEV (ft.)	SLOPE (%)	LS
250	70	28	11.2 (.5)
600	70	11.7	4.3 (.5)

use 7.8

COVER FACTOR

AREA (ac)	COVER TYPE	% COVER	CANOPY (%)	WEIGHTED C
50%	reclaimed	—	—	.5(.15)
50%	P-5	40	25	.5(.14)
				<u>C = .145</u>

EROSION CONTROL FACTOR

$$P = 1.0$$

SEDIMENT INFLOW

$$A = 40(.32)(7.8)(.145)(1.0) = 14.48 \quad \text{ton/acre/year}$$

$$A = 14.48 \left(\frac{1}{2047} \right) (10.6) (.95) = .072 \quad \text{acre-feet/year}$$

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REVISIONS
 BY DATE TO EO
 BY DATE TO EO

BY DATE
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