INSPECTION REPORT

Sedimentation Structure

N6-C

Black Mesa Mine

Navajo County, Arizona

for

PEABODY COAL COMPANY



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INTRODUCTION

Sedimentation Structure N6-C is an earthen embankment, designed and constructed in 1979 by Peabody Coal Company as a temporary sedimentation structure to control runoff and sediment from the disturbed mining areas of the Black Mesa Mine. The location of Structure N6-C is shown on Plate 1, Site Plan.

This inspection report contains information specific to Structure N6-C. Regional site information is presented in the "General Report, Kayenta and Black Mesa Mines, Navajo County, Arizona for Peabody Coal Company," along with the methods and results of analyses used for slope stability, hydrology and hydraulics.

INSPECTION

Structure N6-C was inspected on September 13, 1985 by an interdisciplinary team of engineers from Dames & Moore. The purpose of the inspection was to assess the safety and general condition of the structure with respect to United States Department of Interior, Office of Surface Mining (OSM) regulations.

Dames & Moore's inspection was performed in accordance with applicable 30 CFR 780 and 816 regulations and included a review of the N6-C project files and a field inspection of the structure. The most current information contained in the Peabody Coal Company files includes the 1984 and current survey data and inspections performed in 1984 and 1985 by

Peabody Coal Company. The survey data developed in August 1984 was used in the analyses of the structure. Results of the field inspection are included in this report as Appendix A.

SITE DESCRIPTION

LAND USE

Structure N6-C has a 96.7-acre tributary drainage area and is located near Moenkopi Wash at the Black Mesa Mine. The watershed is classified as 61% Pinion/Juniper and 39% reclaimed.

EMBANKMENT

Structure N6-C is a homogeneous earthen embankment classified as a cross-valley embankment. Physical characteristics of the embankment are listed in the following table:

Structure N6-C

Embankment Residual Shale Soils

Foundation Sandstone

Right Abutment Residual Shale Soils Left Abutment Residual Shale Soils

Height 17 ft

Crest Width 12 ft

Upstream Slope . . . 2.4 H : 1 V

Downstream Slope . . . 3.1 H : 1 V

A cross-section of the embankment is shown on Plate 2, Existing Maximum Cross Section N6-C, A-A'. Grass provides erosion protection on the upstream and downstream slopes of the embankment.

ANALYSES

STABILITY

Structure N6-C is a category B-5 embankment. A standard category B-5 embankment has static and seismic factors of safety equal to or greater than 1.5 and 1.2, respectively, under the following conditions:

- 1. Maximum height = 20 ft
- 2. Maximum upstream slope = 2.0 H : 1 V
- 3. Maximum downstream slope = 2.5 H : 1 V
- 4. Normal pool with steady seepage saturation conditions

The N6-C embankment is lower in height and has flatter slopes than the category standard; therefore, the embankment has factors of safety greater than the design minimum.

HYDROLOGY

The hydrologic analysis was completed using the U.S. Army Corps of Engineers generalized computer program HEC-1, Flood Hydrograph Package. Structure N6-C is not in series with any other structure and therefore the spillway was analyzed using the 25-year, 6-hour storm. The storage capacity of Structure N6-C was analyzed using the 10-year, 24-hour storm.

The following parameters were used in the hydrologic analysis:

1.	Water Course length, L	0.432	mi
2.	Elevation Difference, H	158	ft
3.	Time of Concentration, T	0.140	h
4.	Lag time, 0.6T	0.084	h
5.	SCS Curve Number	83	
6.	Rainfall Depth, 10-year, 24-hour storm .	2.1	in.
	25-year, 6-hour storm	1.9	in.
7.	Drainage Area	96.7	acres

HYDRAULICS

The HEC-1 program was used to evaluate inflow to the sedimentation structure, outflow from the structure and the resulting water surface elevations. The initial conditions and results of the analysis are summarized in the following table.

N6-C HYDRAULICS

Units	10-year 24-hour Storm	25~year 6-hour Storm
Initial Reservoir Volume Condition	Empty	Full to the spillway elevation
Inflow Peak Flow cfs Volume acre-ft	116 6.04	142 4.75
Storage Peak Stage ft	6575.21	
Peak Stage ft Spillway Elevation ft	6578.77	
Peak Storage acre-ft	6.04	
Storage Capacity acre-ft	9.82	
Outflow		
Peak Flow cfs Embankment Crest	0	21
Elevation ft		6579.32
		6581.03
Peak Stage ft		

Spillway Channel

The existing spillway for N6-C has a trapezoidal channel with the following dimensions:

Channel	depth		•						•		•			2.9	ft
Channe1	width				•	•			•				•	35	ft
Channel	length								•					30	ft
Side slo	pes (h	ori	zoi	nta	1	to	<i>r</i> c	/ei	ti	ca	11)).		2:1	
	-														percent

There is presently no erosion protection within the channel.

Outflow Channel

The existing outflow channel for N6-C has a trapezoidal channel with the following dimensions:

There is presently no erosion protection within the channel.

STORAGE CAPACITY

The impoundment volume-elevation curve is based on site specific surveys conducted for Peabody Coal Company's August 1984 inspection, and 1985 resurveys, where available. Additionally, the most current topographic maps available were used in developing Plate 3, Volume-Elevation Curve, N6-C.

The calculations for the sediment load entering Structure N6-C were made utilizing the Universal Soil Loss Equation with the following parameters:

The hydrologic analysis gives the storage volume required to contain the 10-year, 24-hour storm, and the remaining storage volume available for storing sediment. The existing storage capacity of N6-C and the results of the sediment inflow analysis are summarized in the following table.

N6-C STORAGE

Total Storage Capacity 9.82 acre-ft 10-year, 24-hour Storm Inflow 6.04 acre-ft Available Sediment Storage Capacity . 3.78 acre-ft Sediment Inflow Rate 0.519 acre-ft/yr Sediment Storage Life 7 yrs

REMEDIAL COMPLIANCE PLAN

GEOTECHNICS

The inspection of Structure N6-C indicated that the geotechnical problem consist of rill and gully erosion on the upstream and downstream slopes, the side slopes of the spillway and outlet channel, and the right and left abutment and evidence of seepage through the bedrock below the downstream toe of the embankment. Correction of erosion is considered a

periodic maintenance task and does not require remedial action. The seepage through the bedrock beneath the embankment is not considered to be a problem at the present time, however, future inspections should note any increase or any sediment in the flow.

HYDRAULICS

The storage capacity of Structure N6-C is adequate but the spillway capacity is inadequate. The structure does not have an adequate outflow channel. The bottom elevation of the existing spillway channel should be lowered to elevation 6576.70 feet while maintaining the bottom width of 30 feet as shown on Plate 5. A trapezoidal outflow channel with the same bottom width as the spillway and a stilling basin should be constructed along the alignment shown in Plate 1. The channel and stilling basin profile is shown in Plate 4 and required dimensions are shown in Plate 5 and Plate 6. The spillway, outflow channel and stilling basin should be protected against erosion using geotextile and riprap as shown in Plate 5.

Lowering the spillway elevation to 6576.70 feet decreases the storage capacity and increases the freeboard. The analysis of these conditions is summarized in the following table.

N6-C HYDRAULICS FOR REDESIGNED SPILLWAY

Units	10-year 24-hour Storm	25-year 6-hour Storm
Initial Reservoir Volume Condition	Empty	Full to the spillway elevation
Inflow Peak Flow cfs Volume acre-ft	116 6.04	142 4.75
Storage Peak Stage ft Spillway Elevation ft Peak Storage acre-ft Storage Capacity acre-ft Available Sediment Storage Capacity acre-ft Sediment Inflow Rate . acre-ft/yr Sediment Storage Life. yrs	6575.21 6576.70 6.04 7.55 1.51 0.519	
Outflow Peak Flow cfs Embankment Crest Elevation ft Peak Stage ft Freeboard ft	0 	84 6579.32 6578.21 1.11
Spillway Channel Flow Depth ft Critical Velocity fps Manning's "n"	 	1.51 4.3 0.61
Outflow Channel Slope	 	Section I Section II 2 16 3.9 7.4 0.68 0.36 0.040 0.040

* * *

The following plates and appendix are attached and complete this inspection report.

Plate 1 - Site Plan N6-C

Plate 2 - Existing Maximum Cross Section N6-C, A-A'

Plate 3 - Volume-Elevation Curve N6-C

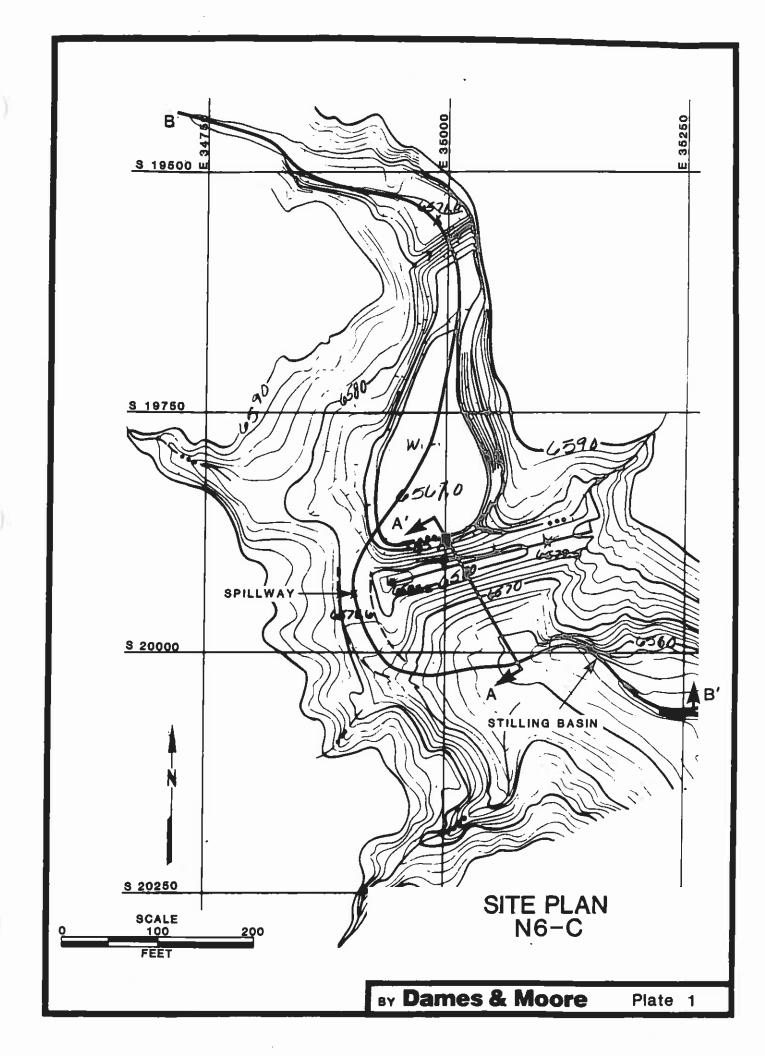
Plate 4 - Channel Profile N6-C, B-B'

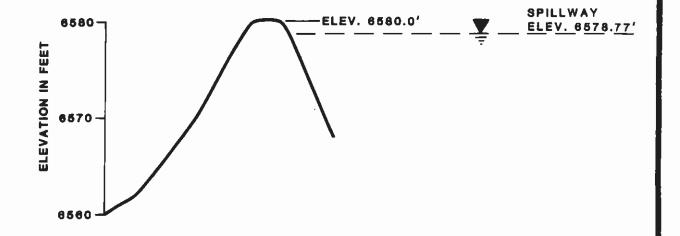
Plate 5 - Spillway and Outflow Channel Cross Section N6-C

Plate 6 - Spillway Stilling Basin Plan N6-C

Appendix A - Inspection Check List

Appendix B - Hydrology and Hydraulic Calculations







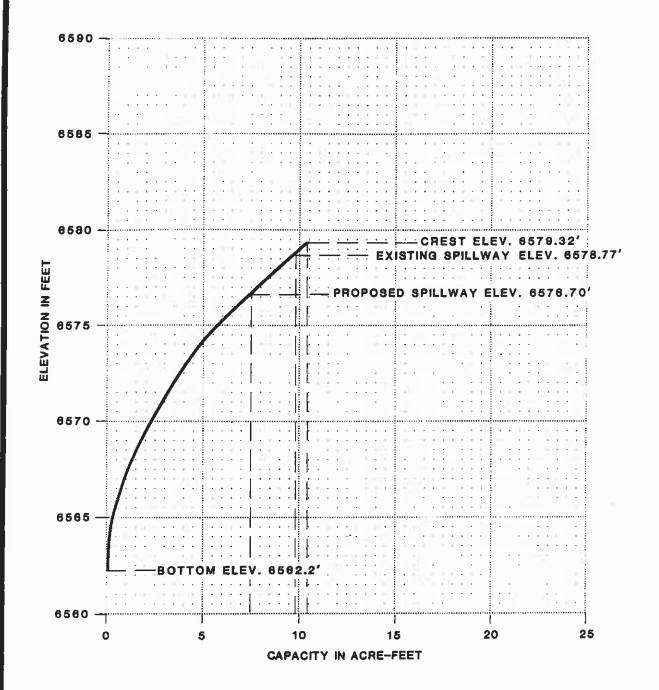
EXISTING
MAXIMUM CROSS-SECTION
A-A'
N6-C

FOR LOCATION SEE PLATE 1

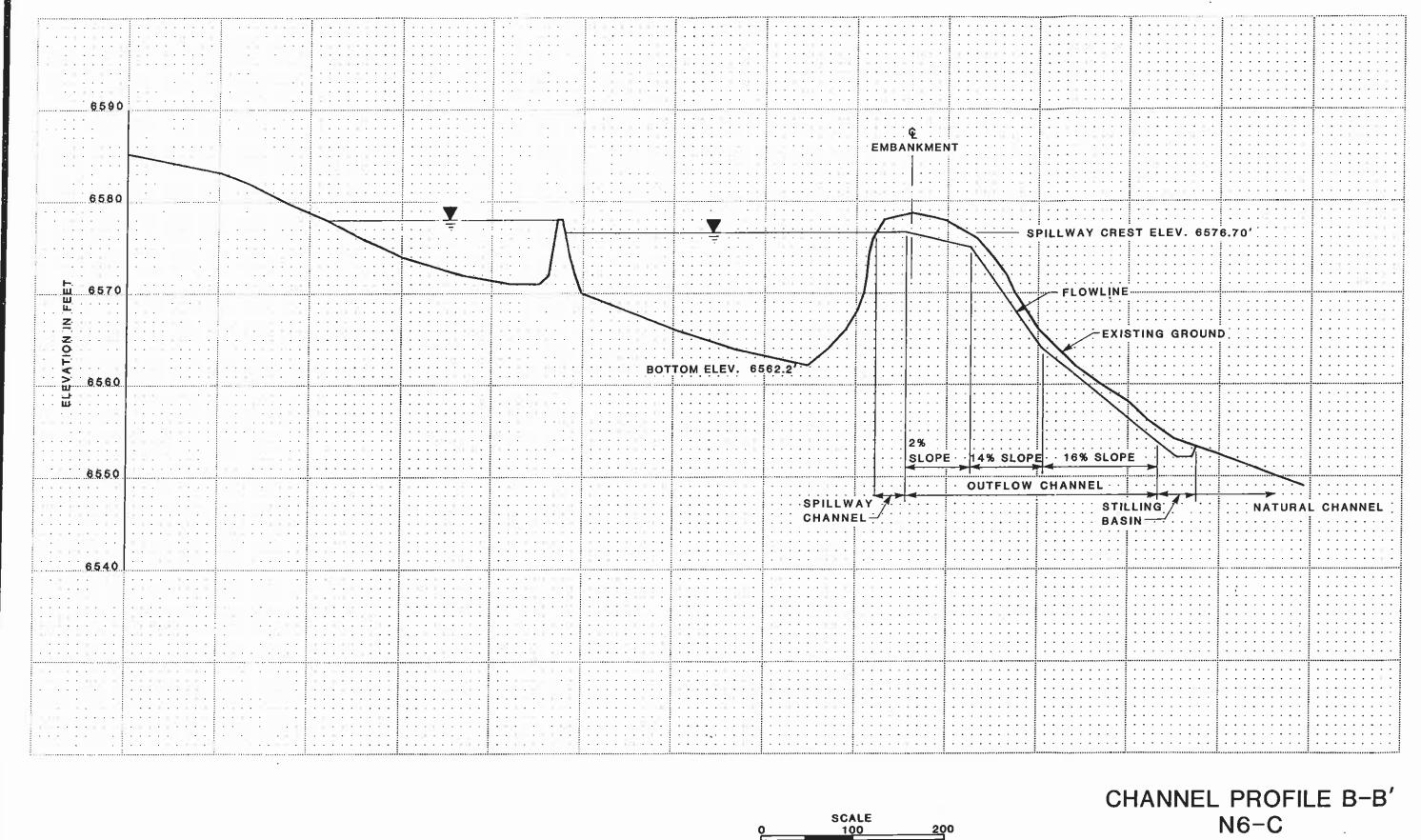
BY Dames & Moore

Plate

2

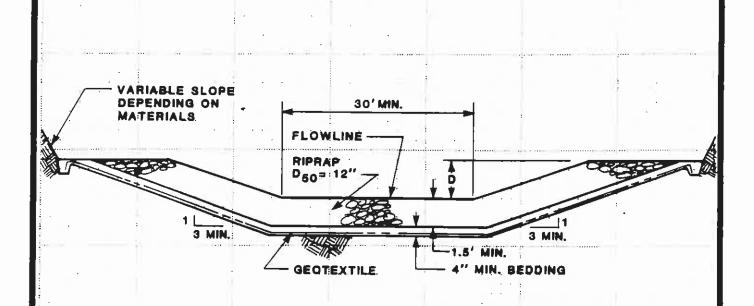


VOLUME-ELEVATION CURVE N6-C



BY Dames & Moore

Plate



SPILLWAY CHANNEL

D = 2.6'

LENGTH = 30'

FLOWLINE ELEV. = 8576.70'

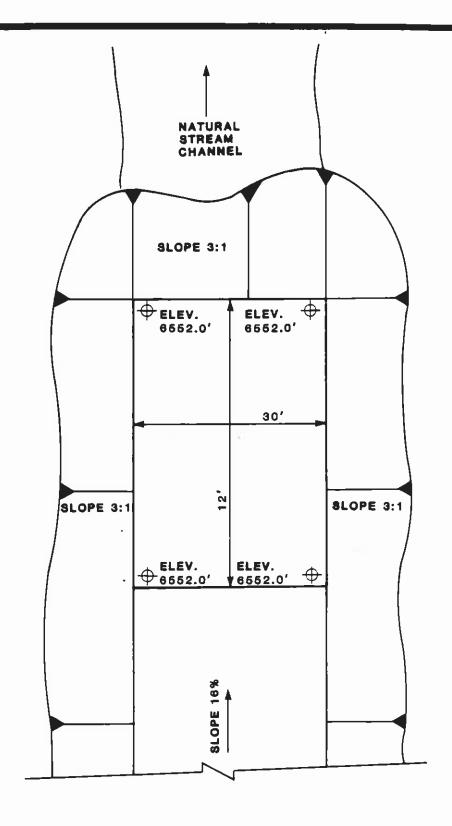
OUTFLOW CHANNEL

D = 2.0'

SPILLWAY AND OUTFLOW CHANNEL CROSS SECTION N6-C

BY Dames & Moore

Plate 5



MINIMUM HEIGHT OF RIPRAP ALONG SIDEWALLS ABOVE THE BASIN FLOOR = 3.4'

MINIMUM DEPTH OF BASIN FLOOR BELOW NATURAL STREAMBED = 1.8' SPILLWAY STILLING BASIN PLAN N6-C

APPENDIX A INSPECTION CHECK LIST

Sediment Impoundment Name: NG-C
Page: 4

INSPECTION CHECK LIST

Timene	YES	NO	REMARKS
ITEM	120	.,,	
1. CREST			12' W.
a. Any visual settlements?		X	
b. Misalignment?		X	
c. Cracking?		X	
<u> </u>			229
2. UPSTREAM SLOPE			23°
a. Adequate grass cover?		X	
b. Any erosion?	\times		Rills
c. Are trees growing on slope?		X	<u> </u>
d. Longitudinal cracks?		\times	
e. Transverse cracks?		\times	
f. Adequate riprap protection?		X	
g. Any stone deterioration?			NA
h. Visual depressions or bulges?		X	
i. Visual settlements?		X	
j. Animal burrows?		X	
3. DOWNSTREAM SLOPE			18°
a. Adequate grass_cover?	1	X	
b. Any erosion?	X		Rills
c. Are trees growing on slope?		X	
d. Longitudinal cracks?		$\overline{\mathbf{x}}$	
e. Transverse cracks?		X	
f. Visual depressions or bulges?		X	
q. Visual settlements?	1	V	
h. Is the toe drain dry?			NA
i. Are the relief wells flowing?			NA
j. Are boils present at the toe?	\vdash	X	
k. Is seepage present?	X		beyond toe, thru Rock hish vegetation
1. Animal burrows?		V	1
I. MITMAT DULLOWS:		1	
4. ABUIMENT CONTACT. RIGHT	,		
a. Any erosion?	X		luto spill way Rills + I gulley sur.
b. Visual differential movement?		X	
c. Any cracks noted?		X	
d. Is seepage present?		×	
e. Type of Material?			gray sm
5. ABUIMENT CONTACT. LEFT			
a. Any erosion?	X		I gulley into poud u.s. of dam
b. Visual differential movement?		X	
c. Any cracks noted?		X	
d. Is seepage present?		×	
e. Type of Material?			brown 5M
e. type or interior.			111111111111111111111111111111111111111

Sediment Impoundment Name: NG-C
Page: 5

ITEM	YES	NO	REMARKS
6. SPILLWAY/NORMAL			
a. Location:		1	
Left abutment?			
Right abutment?	X		
Crest of Embankments?			
b. Approach Channel:		X	
Are side slopes eroding?			
Are side slopes sloughing?			I NA
Bottom of channel eroding?			
Obstructed?			
Erosion protection?			
c. Spillway Channel:	\rightarrow		35'W (1% Slape 2.9' below (rost 30)
Are side slopes eroding?	T	1	Rills from RA
Are side slopes sloughing?	1	X	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Bottom of channel eroding?	1	 Q	
Obstructed?	+		
Erosion protection?	+	 	
d. Outflow Channel:	 ×		35'W. 30 From 3 to 8
Are side slopes eroding?	+(>	\vdash	Gulley from RA
Are side slopes sloughing?	- × -	$\overline{}$	Guney from 109
Bottom of channel eroding?	X		Rills
Bottom of channel eroding?	- ^-		Kills
Obstructed?		X	
Erosion protection?	-	X	
e. Weir:	—	X	
Condition?			
			/
7. SPILLWAY/EMERGENCY			
			NA /
a. Location:			NA /
Left abutment?			
Right abutment?			
Crest of Embankments?			
b. Approach Channel:			
Are side slopes eroding?			
Are side slopes sloughing?			/
Bottom of channel eroding?			
Obstructed?			/
Erosion protection?			
c. Spillway Channel:			
Are side slopes eroding?			
Are side slopes sloughing?			
Bottom of channel eroding?			
Obstructed?			
	+		
Erosion protection?			
d. Outflow Channel:			
Are side slopes eroding?			
Are side slopes sloughing?			
Bottom of channel eroding?	\perp		/
Obstructed?	\perp		
Erosion protection?			
e. Weir:			
Condition?	1 /		

Sediment Impoundment Name: Name: Name: 6

ITEM	YES	NO	REMARKS	
3. IMPOUNDMENT				
a. Sinkholes?		M	(Elev.)	feet
b. Water present?	X		(Elev.)	feet
c. Siltation?	×	_		
d. Watershed matches soil m		X		
Evidence of part beyond toe of	7.5') Hg		Hora Rock	of Na-c
	-			
			·	
			_	

Canopy 35 %.
Grand 55%

APPENDIX B HYDROLOGY AND HYDRAULIC CALCULATIONS

FILE YEABODY COM CO 10139-011-22
SUBJECT SEDIMENT FOND HYDROLOGY

NG-C SHEET OF

TIME OF CONCENTRATION

ELEVATION DIFFERENCE = 6737 - 6579 = 158 ft.WATER (OURSE LEDWITH = 5.7 (400)= 2290 ft. = 0.432 mi. $T_{c} = \left(\frac{11.9 (0.432)^{3}}{158}\right)^{0.385} = 0.140 \text{ hr.}$ LAW TIME = $0.6T_{c} = 0.084 \text{ hr.}$

SCS CUEVE NUMBER

DRAINAGE	COUER	Hydrologic	Soil	WEIGHTED
ARTA (ac)	TYPE	(ONDITION)	TYPE	CURVE NUMBER
58.5	P-J	average	. D	83 (,61)
38.2	reclaimed (post bu)	fair		81 (,39)
	-			82.2
			3	use 83
		61% EH # 3		

DRAINAGE BASIN AREA

96,7 ACOS 0, 151 SO HILD

FILE	TABULY	WAL	C	10:54-0: - 00	
SUBJECT	SEDIM	いとて	工工	FLOW	
N6	- C			SHEETOF.	

UNIVERSAL SOIL LOSS EQUATION

RAINPALL FACTOR

R= 40

SOIL ERODIBILITY FACTOR

K= .298

SLOPE FACTOR

LENGTH (FL.)	DELEV (f1)	Sw0E (%)	<u>LS</u>
450	60	13.3	4.51 (.2)
700	110	15.7	7,30 (,2)
758.	230	30.7	22.58 (1) 4.23 (15)
600	70	11,7	
			= 674

COVER FACTOR

EROSION CONTROL FACTOR

P= 1.0

SEDIMENT INFLOW

A =
$$40(.298)(6.74)(.144)(1.0) = 11.57$$
 ton | acre | year
A = $(11.57)(.264.7)(.95) = .519$ acre-feet | year
Dames & Moore