INSPECTION REPORT

Sedimentation Structure

N1-AC

Kayenta Mine

Navajo County, Arizona

for

PEABODY COAL COMPANY



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INTRODUCTION

Sedimentation Structure N1-AC is an earthen embankment, designed and constructed in 1980 by Peabody Coal Company as a temporary sedimentation structure to control runoff and sediment from the disturbed mining areas of the Kayenta Mine. The location of Structure N1-AC is shown on Plate 1, Site Plan.

This inspection report contains information specific to Structure N1-AC. Regional site information is presented in the "General Report, Kayenta and Black Mesa Mines, Navajo County, Arizona for Peabody Coal Company," along with the methods and results of analyses used for slope stability, hydrology and hydraulics.

INSPECTION

Structure N1-AC was inspected on September 5, 1985 by an interdisciplinary team of engineers from Dames & Moore. The purpose of the inspection was to assess the safety and general condition of the structure with respect to United States Department of Interior, Office of Surface Mining (OSM) regulations.

Dames & Moore's inspection was performed in accordance with applicable 30 CFR 780 and 816 regulations and included a review of the N1-AC project files and a field inspection of the structure. The most current information contained in the Peabody Coal Company files includes the 1984 and current survey data and inspections performed in 1984 and 1985 by

Peabody Coal Company. The survey data developed in August 1984 was used in the analyses of the structure. Results of the field inspection are included in this report as Appendix A.

SITE DESCRIPTION

LAND USE

Structure N1-AC has a 118.8-acre tributary drainage area and is located near Yellow Water Canyon at the Kayenta Mine. The watershed is classified as 45% Pinion/Juniper, 38% reclaimed, 17% disturbed.

EMBANKMENT

Structure N1-AC is a homogeneous earthen embankment classified as a in-wash embankment. Physical characteristics of the embankment are listed in the following table:

Structure N1-AC

Embankment Residual Shale Soils Foundation Residual Shale Soils Right Abutment . . . Residual Shale Soils Left Abutment . . . Residual Shale Soils Height 10.8 ft Crest Width 17 ft Upstream Slope 1.9 H : 1 V Downstream Slope . . . 2.5 H : 1 V

A cross-section of the embankment is shown on Plate 2, Existing Maximum Cross Section NI-AC, A-A'. Grass provides erosion protection on the upstream and downstream slopes of the embankment.

ANALYSES

STABILITY

Structure N1-AC is a category B-1 embankment. A standard category B-1 embankment has static and seismic factors of safety equal to or greater than 1.5 and 1.2, respectively, under the following conditions:

- 1. Maximum height = 15 ft
- 2. Maximum upstream slope = 1.75 H : 1 V
- 3. Maximum downstream slope = 2.5 H : 1 V
- 4. Normal pool with steady seepage saturation conditions

The N1-AC embankment is lower in height and has flatter slopes than the category standard; therefore, the embankment has factors of safety greater than the design minimum.

HYDROLOGY

The hydrologic analysis was completed using the U.S. Army Corps of Engineers generalized computer program HEC-1, Flood Hydrograph Package. Structure N1-AC is not in series with any other structure and therefore the spillway was analyzed using the 25-year, 6-hour storm. The storage capacity of Structure N1-AC was analyzed using the 10-year, 24-hour storm.

The following parameters were used in the hydrologic analysis:

1.	Water Course length, L 0.432	mi
2.	Elevation Difference, H 154	ft
3.	Time of Concentration, T 0.141	h
4.	Lag time, 0.6T 0.085	h
5.	SCS Curve Number 87	
6.	Rainfall Depth, 10-year, 24-hour storm . 2.1	in.
	25-year, 6-hour storm 1.9	in.
7	Drainage Area	actes

HYDRAULICS

The HEC-1 program was used to evaluate inflow to the sedimentation structure, outflow from the structure and the resulting water surface elevations. The initial conditions and results of the analysis are summarized in the following table.

N1-AC HYDRAULICS

Units	10-year 24-hour Storm	25-year 6-hour Storm
Initial Reservoir Volume Condition	Empty	Full to the spillway elevation
Inflow Peak Flow cfs Volume acre-ft	189 9.80	239 8.42
Storage		
Peak Stage ft	6535.84	
Spillway Elevation ft	6538.80	
Peak Storage acre-ft	9.82	
Storage Capacity acre-ft	16.3	
Outflow		
Peak Flow cfs Embankment Crest	0	102
Elevation ft		6540.80
Peak Stage ft		6540.46
Freeboard ft		0.34

Spillway Channel

The existing spillway for NI-AC has a trapezoidal channel with the following dimensions:

There is presently no erosion protection within the channel.

Outflow Channel

The existing outflow channel for N1-AC has a U-shaped channel with the following dimensions:

There is presently no erosion protection within the channel.

STORAGE CAPACITY

The impoundment volume-elevation curve is based on site specific surveys conducted for Peabody Coal Company's August 1984 inspection, and 1985 resurveys, where available. Additionally, the most current topographic maps available were used in developing Plate 3, Volume-Elevation Curve, NI-AC.

The calculations for the sediment load entering Structure N1-AC were made utilizing the Universal Soil Loss Equation with the following parameters:

The hydrologic analysis gives the storage volume required to contain the 10-year, 24-hour storm, and the remaining storage volume available for storing sediment. The existing storage capacity of N1-AC and the results of the sediment inflow analysis are summarized in the following table.

N1-AC STORAGE

Total Storage Capacity		16.3	acre-ft
10-year, 24-hour Storm Inflow		9.82	acre-ft
Available Sediment Storage Capacity	•	6.48	acre-ft
Sediment Inflow Rate		1.62	acre-ft/yr
Sediment Storage Life		4	yrs

REMEDIAL COMPLIANCE PLAN

GEOTECHNICS

The inspection of Structure N1-AC indicated that the geotechnical problems consist of rill on the upstream and downstream slopes; the side slopes of the spillway and outlet channel; and the right abutment and cracks at the upstream edge of the crest towards the left abutment. Correction of erosion is considered a periodic maintenance task and does not require

remedial action. The cracks in the crest should be repaired by excavating to the bottom of the cracks and replacing with compacted fill.

HYDRAULICS

The storage capacity of Structure N1-AC is adequate but the spillway capacity is inadequate. The structure does not have an adequate outflow channel. The bottom elevation of the existing spillway channel should be lowered to elevation 6538.0 feet while maintaining the bottom width of 50 feet as shown on Plate 5. A trapezoidal outflow channel with the same bottom width as the spillway should be constructed along the alignment shown in Plate 1. The channel profile is shown in Plate 4 and required dimensions are shown in Plate 5 and Plate 6. The spillway, outflow channel and stilling basin should be protected against erosion using geotextile and riprap as shown in Plate 5.

Lowering the spillway elevation to 6538.0 feet decreases the storage capacity and increases the freeboard. The analysis of these conditions is summarized in the following table.

N1-AC HYDRAULICS FOR REDESIGNED SPILLWAY

Units	10-year 24-hour Storm	
Initial Reservoir Volume Condition	Empty	Full to the spillway elevation
Inflow Peak Flow cfs Volume acre-ft	189 9.80	239 8.42
Storage Peak Stage ft Spillway Elevation ft Peak Storage acre-ft Storage Capacity acre-ft Available Sediment Storage Capacity acre-ft Sediment Inflow Rate . acre-ft/yr Sediment Storage Life . yrs	6538.81 6538.00 9.82 14.53 4.71 1.62	6539.67
Outflow Peak Flow cfs Embankment Crest Elevation ft Peak Stage ft Freeboard ft	 	107 6540.80 6539.67 1.13
Spillway Channel Flow Depth ft Critical Velocity fps Manning's "n"	 	1.67 4.0 0.040
Outflow Channel Slope	 	Section I Section II 48 3 9.3 4.0 0.22 0.51 0.040 0.040

* * *

The following plates and appendix are attached and complete this inspection report.

Plate 1 - Site Plan N1-AC

Plate 2 - Existing Maximum Cross Section NI-AC, A-A'

Plate 3 - Volume-Elevation Curve N1-AC

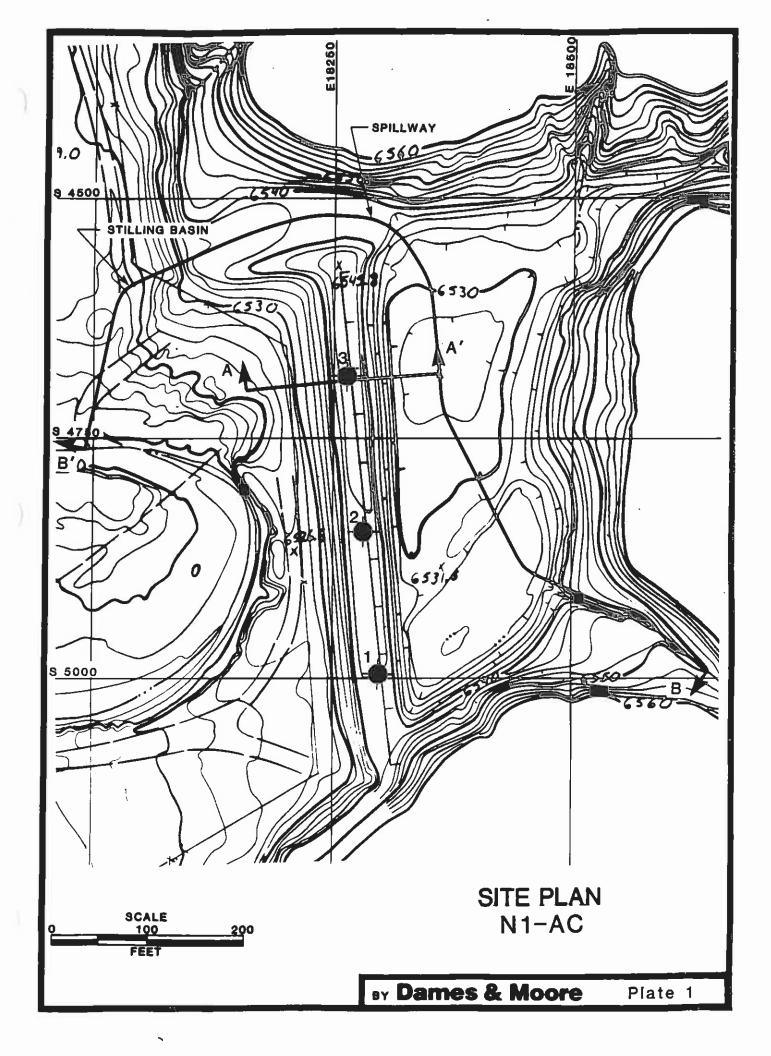
Plate 4 - Channel Profile N1-AC, B-B'

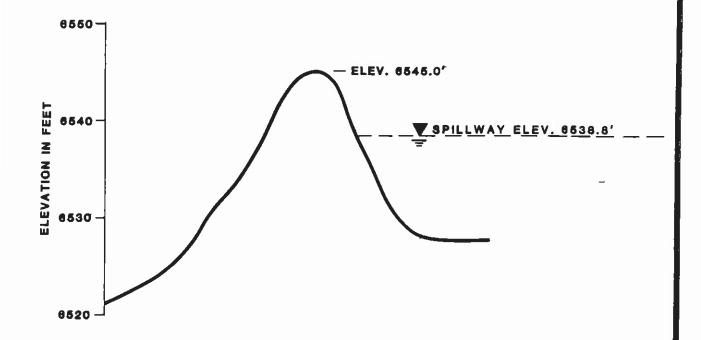
Plate 5 - Spillway and Outflow Channel Cross Section N1-AC

Plate 6 - Spillway Stilling Basin Plan N1-AC

Appendix A - Inspection Check List

Appendix B - Hydrology and Hydraulic Calculations





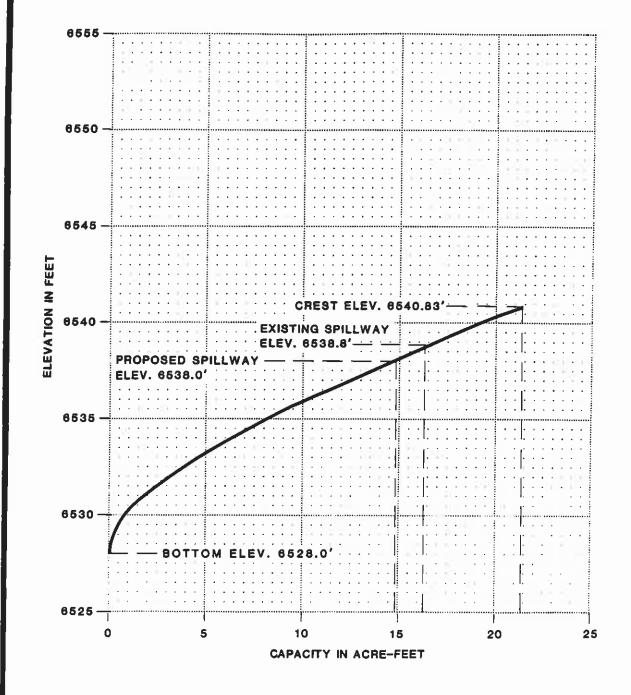


FOR LOCATION SEE PLATE 1

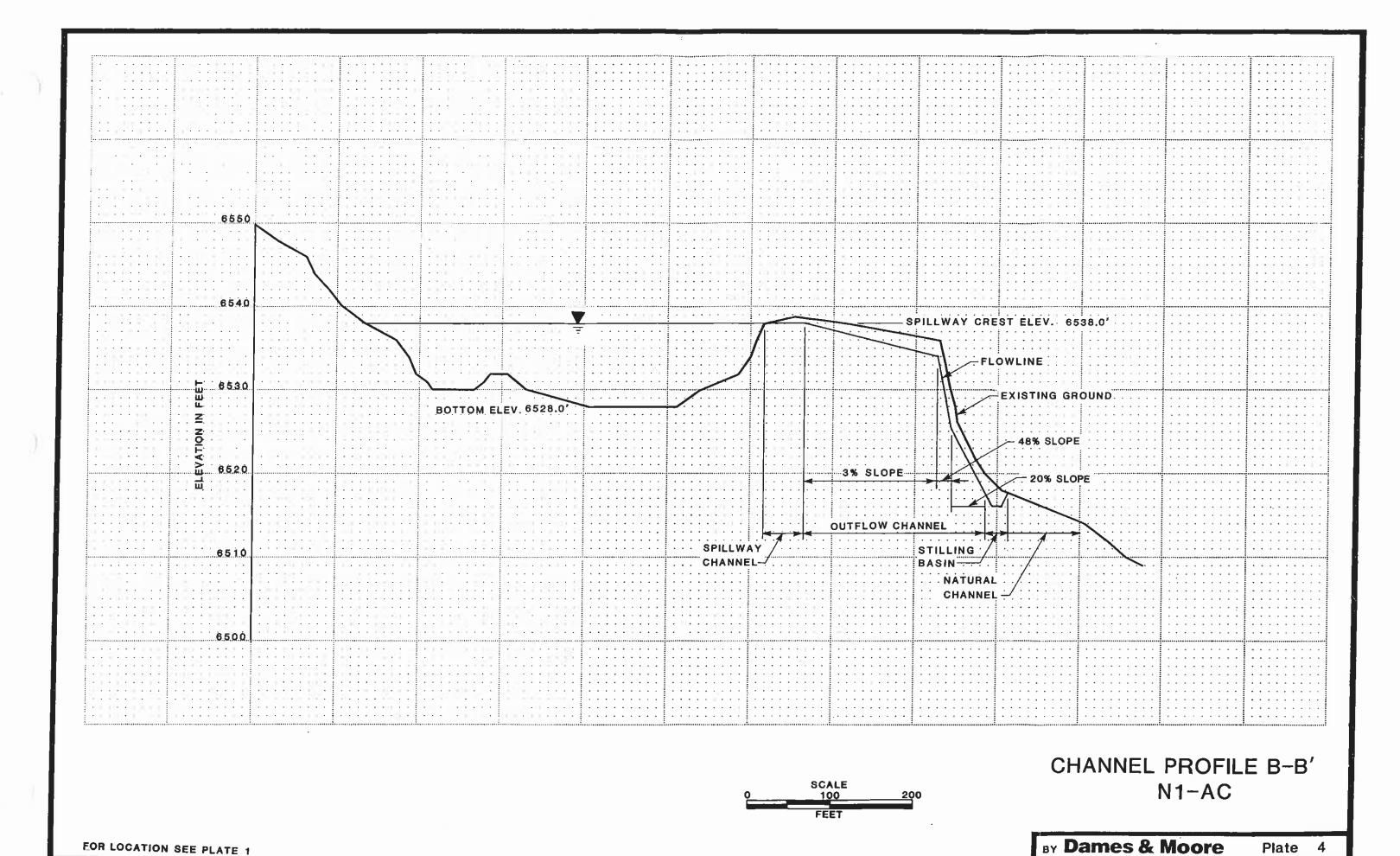
EXISTING
MAXIMUM CROSS-SECTION
A-A'
N1-AC

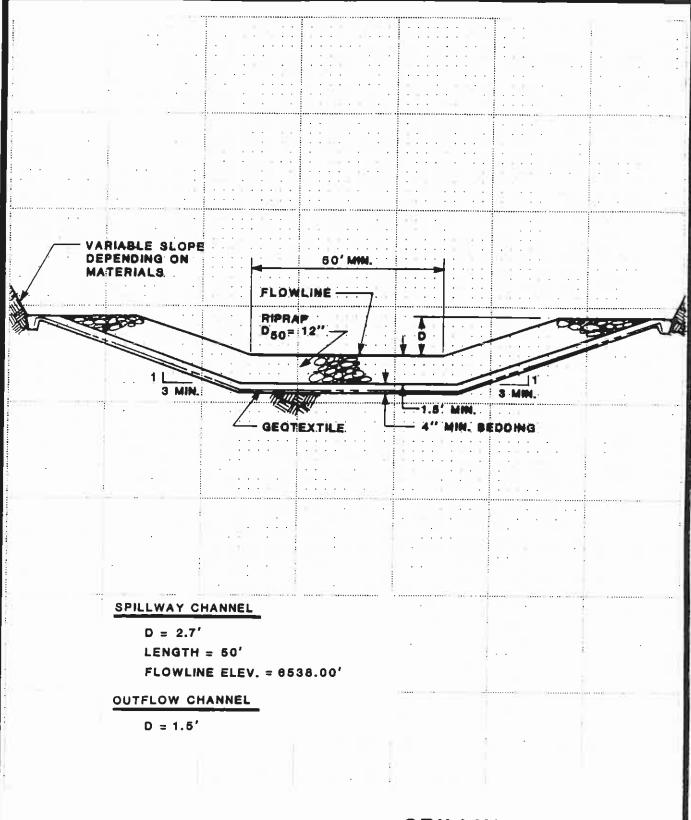
BY Dames & Moore

Plate 2



VOLUME-ELEVATION CURVE N1-AC

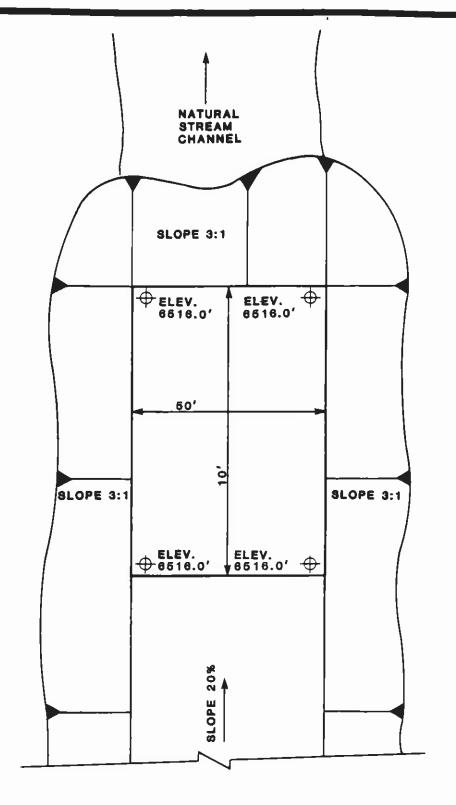




SPILLWAY AND OUTFLOW CHANNEL CROSS SECTION N1-AC

BY Dames & Moore

Plate :



MINIMUM HEIGHT OF RIPRAP ALONG SIDEWALLS ABOVE THE BASIN FLOOR = 2.9'

MINIMUM DEPTH OF BASIN FLOOR BELOW NATURAL STREAMBED = 1.5' SPILLWAY STILLING BASIN PLAN N1-AC

APPENDIX A INSPECTION CHECK LIST

Sediment Impoundment Name: N/-AC
Page: 4

INSPECTION CHECK LIST

ITEM	YES	NO	REMARKS
			17'
1. CREST			17
a. Any visual settlements?	_	\sim	
b. Misalignment?	<u> </u>	\succeq	
c. Cracking?		\simeq	
2. UPSTREAM SLOPE			28° Ragged unen
a. Adequate grass cover?	\times		(60°60
b. Any erosion?	X		(2:115
c. Are trees growing on slope?		X	
d. Longitudinal cracks?	\geq		At edge of event 12" deep
e. Transverse cracks?		\bowtie	_
f. Adequate riprap protection?	${}$		Grass
g. Any stone deterioration?			NA
h. Visual depressions or bulges?		$\overline{\mathbf{x}}$	
i. Visual settlements?		X	
. Animal burrows?		X	E
			22°
3. DOWNSTREAM SLOPE			
a. Adequate grass cover?	\times		75%
b. Any erosion?	\times		Kills
c. Are trees growing on slope?	,	×	
d. Longitudinal cracks? .		区	1
e. Transverse cracks?		X	
f. Visual depressions or bulges?		\times	
q. Visual settlements?		×	
h. Is the toe drain dry?			NA .
i. Are the relief wells flowing?			NA
j. Are boils present at the toe?	i	\supset	
k. Is seepage present?		$\overline{\times}$	
1. Animal burrows?		X	
4. ABUTMENT CONTACT. RIGHT			Rills
	_		
a. Any erosion?	\prec	, ,	INTO Spilway
b. Visual differential movement?		X	
c. Any cracks noted?		$ \mathbf{X} $	
d. Is seepage present?		\geq	7
e. Type of Material?			Kock
5. ABUIMENT CONTACT. LEFT			
a. Any erosion?		X	
b. Visual differential movement?		X	
c. Any cracks noted?	_	\mathbf{x}	
d. Is seepage present?		X	
e. Type of Material?	_		Rock

Sediment Impoundment Name: Nam

ITEM	YES	NO	REMARKS
6. SPILLWAY/NORMAL			
a. Location:			
Left abutment?			
Right abutment?	-		
Crest of Embankments?		-	
b. Approach Channel:		$\overline{}$	
Are side slopes eroding?			
Are side slopes sloughing?		1	No
Bottom of channel eroding?			
Obstructed?			
Erosion protection?		_	4
c. Spillway Channel:	\rightarrow	Н	8' below crest 45'W.
Are side slopes eroding?	$\overline{\langle}$		Rills
Are side slopes sloughing?		$\overline{\mathbf{x}}$	
Bottom of channel eroding?		X	
Obstructed?			
Erosion protection?		\bigcirc	-
d. Outflow Channel:	$\overline{}$		· · · · · · · · · · · · · · · · · · ·
Are side slopes eroding?			Rills
Are side slopes sloughing?	 	$\overline{\mathbf{z}}$	
Bottom of channel eroding?			at end
Obstructed?		\times	
Erosion protection?			some rock at end
e. Weir:		X	70-41- 01-31
Condition?	,		
7. SPILLWAY/EMERGENCY			
•			110
a. Location:			NA
Left abutment?			
Right abutment?			
Crest of Embankments?			
b. Approach Channel:			
Are side slopes eroding?			
Are side slopes sloughing?			
Bottom of channel eroding?			
Obstructed?			
Erosion protection?			
c. Spillway Channel:			
Are side slopes eroding?			
Are side slopes sloughing?			
Bottom of channel eroding?			/
Obstructed?			
Erosion protection?			/
d. Outflow Channel:			/
Are side slopes eroding?			
Are side slopes sloughing?		Z	
Bottom of channel eroding?			
Obstructed?	1/		
Erosion protection?	1/		<u> </u>
e. Weir:	7		
Condition?			
			

Sediment Impoundment Name: Name: Name: 6

ITEM	YES	NO	REMARKS	
3. IMPOUNDMENT				
a. Sinkholes?		\times	(Elev.)	feet
b. Water present?	$\geq \leq$		(Elev.)	feet
c. Siltation?	\times		modirate	_
d. Watershed matches soil map?		\times		
May be due to poor	20	المح	of crest 12" deep. - compaction of - building crest.	
			•	
- -		_		

Ground cover 475 %. Conopy over 425 %

APPENDIX B HYDROLOGY AND HYDRAULIC CALCULATIONS

REVISIONS
BY ______ DATE _____ TO EO ____
BY _____ DATE _____ TO EO ____

TIME OF CONCENTRATION

ELEVATION DIFFERENCE = 6693 - 6539 = 154 ft.

WATER COURSE LEDOUTH = 5.7(400) = 2280 ft = 0.432 mi.

$$T_c = \left(\frac{11.9 (0.43)^3}{154}\right)^{0.385} = 0.141 \text{ hr. } 4$$

LAG TIME = 0.6To = 0.085 ho 14

Note: SEE CALCULATIONS
ON BACK.

SCS CURUG NUMBER

DRAINAGE	COUER	Hydrocock	Soll	WEIGHTED
ARFA (ac)	TYPE	(ONDITION)	TYPE	CURVE NUMBER
7.4	Distribed		P	(.06) 94
45.2	Reclaimed			(38) 87
52.9	P-J	average	D	(.45)83
13.3	Grand Road		D	(.11) 91
		il mom		

3870 #35 6270 #24 use 87

S, $DOL^A M$ DATE 9-12-8 SCHECKED BY

DRAINAGE BASIN AREA

118.8 ACRE 0.186 SO MILE

T0 E0	T0 E0
DATE.	DATE.
Σ.	\succeq

COPY TO EO

UNIVERSAL SOIL LOSS ERMATION

RAINFALL FACTOR

R= 40

Soil ELODIBILITY FACTOR

K= ,26

SLOPE FACTOR

LEWGIH(fi)	DELEV (f1)	Sw02 (%)	<u>LS</u>
(100	3 0 ™	3%.	,59 (.3)
400	30	89.	1.98 (.2)
400	180	45%	22,00 (,4)
300	30	10%	2.37 (.1)

use 9.6

COVER FACTOR

ARTA (a	c.) WER TYPE	% (33=2	CANDPY (9)	WEIGHTED C
.670	disturbel			(.06)(1.0)
38%	neclaimed			(.38 (.15)
45%	P-J	40	25	(.45)(.14)
13%	road			(.13)(1.0)
6				31

EROSION CONTROL FACTOR

P=1.0

SEDIMENT INFLOW

Dames & Moore