INSPECTION REPORT

Sedimentation Structure

J28-D

Kayenta Mine

Navajo County, Arizona

for

PEABODY COAL COMPANY

Dames & Moore
10139-011-22

TABLE OF CONTENTS

INTRODUCTION

Sedimentation Structure J28-D is an earthen embankment, designed and constructed in 1983 by Peabody Coal Company as a temporary sedimentation structure to control runoff and sediment from the disturbed mining areas of the Kayenta Mine. The location of Structure J28-D is shown on Plate 1, Site Plan.

This inspection report contains information specific to Structure J28-D. Regional site information is presented in the "General Report, Kayenta and Black Mesa Mines, Navajo County, Arizona for Peabody Coal Company," along with the methods and results of analyses used for slope stability, hydrology and hydraulics.

INSPECTION

Structure J28-D was inspected on September 12, 1985 by an inter-disciplinary team of engineers from Dames & Moore. The purpose of the inspection was to assess the safety and general condition of the structure with respect to United States Department of Interior, Office of Surface Mining (OSM) regulations.

Dames & Moore's inspection was performed in accordance with applicable 30 CFR 780 and 816 regulations and included a review of the J28-D project files and a field inspection of the structure. The most current information contained in the Peabody Coal Company files includes the 1984 and current survey data and inspections performed in 1984 and 1985 by

Peabody Coal Company. The survey data developed in August 1984 was used in the analyses of the structure. Results of the field inspection are included in this report as Appendix A.

SITE DESCRIPTION

LAND USE

Structure J28-D has a 30.4-acre tributary drainage area and is located near Moenkopi Wash at the Kayenta Mine. The watershed is classified as 76% disturbed and 24% Pinion/Juniper.

EMBANKMENT

Structure J28-D is a homogeneous earthen embankment classified as a sidehill embankment. Physical characteristics of the embankment are listed in the following table:

Structure J28-D

Embankment	Residual Shale Soils
Foundation	Residual Shale Soils
Right Abutment	Residual Shale Soils
Left Abutment	Residual Shale Soils
Height	14.5 ft
Crest Width	15 ft
Upstream Slope	2.6 H : 1 V
Downstream Slope	2.4 H : 1 V

A cross-section of the embankment is shown on Plate 2, Existing Maximum Cross Section J28-D, A-A'. Grass provides erosion protection on the downstream slope of the embankment.

ANALYSES

STABILITY

Structure J28-D is a category B-1 embankment. A standard category B-1 embankment has static and seismic factors of safety of 1.5 and 1.2, respectively, under the following conditions:

1. Maximum height = 20 ft
2. Maximum upstream slope = 2.0 H : 1 V
3. Maximum downstream slope = 2.5 H : 1 V
4. Normal pool with steady seepage saturation conditions

The J28-D embankment is lower in height; however, the downstream slope is steeper than the category standard; therefore, the embankment has factors of safety less than the design minimum.

HYDROLOGY

The hydrologic analysis was completed using the U.S. Army Corps of Engineers generalized computer program HEC-1, Flood Hydrograph Package. Structure J28-D is not in series with any other structure and therefore the spillway was analyzed using the 25-year, 6-hour storm. The storage capacity of Structure J28-D was analyzed using the 10-year, 24-hour storm.

The following parameters were used in the hydrologic analysis:

1.	Water Course length, L	0.227	mi
2.	Elevation Difference, H	106	ft
3.	Time of Concentration, T_c	0.078	h
4.	Lag time, $0.6T_c$	0.047	h
5.	SCS Curve Number	88	
6.	Rainfall Depth, 10-year, 24-hour storm	2.1	in.
	25-year, 6-hour storm	1.9	in.
7.	Drainage Area	30.4	acres

HYDRAULICS

The HEC-1 program was used to evaluate inflow to the sedimentation structure, outflow from the structure and the resulting water surface elevations. The initial conditions and results of the analysis are summarized in the following table.

	Units	10-year 24-hour Storm	25-year 6-hour Storm
Initial Reservoir Volume Condition		Empty	Full to the spillway elevation
Inflow			
Peak Flow	cfs	67	82
Volume	acre-ft	2.79	2.31
Storage			
Peak Stage	ft	6779.10	6789.70
Spillway Elevation . .	ft	6788.96	—
Peak Storage	acre-ft	2.83	—
Storage Capacity . . .	acre-ft	17.6	—
Outflow			
Peak Flow	cfs	0	6
Embankment Crest Elevation	ft	—	6791.10
Peak Stage	ft	—	6789.72
Freeboard	ft	—	1.38
Spillway Channel			
Flow Depth	ft	—	0.76
Critical Velocity. . .	fps	—	2.1
Manning's "n"		—	0.035
Outflow Channel			
Slope	%	—	6
Normal Velocity. . . .	fps	—	2.5
Normal Depth	ft	—	0.12
Manning's "n"		—	0.035

Spillway Channel

The existing spillway for J28-D has a trapezoidal channel with the following dimensions:

Channel depth	3.0	ft
Channel width	17	ft
Channel length	25	ft
Side slopes (horizontal to vertical)	2:1	
Average exit slope	0	percent

There is presently no erosion protection within the channel.

Outflow Channel

The existing outflow channel for J28-D has a U-shaped channel with the following dimensions:

Channel width	17	ft
Channel length	120	ft
Average exit slope	2	percent

There is presently no erosion protection within the channel.

STORAGE CAPACITY

The impoundment volume-elevation curve is based on site specific surveys conducted for Peabody Coal Company's August 1984 inspection, and 1985 resurveys, where available. Additionally, the most current topographic maps available were used in developing Plate 3, Volume-Elevation Curve, J28-D.

The calculations for the sediment load entering Structure J28-D were made utilizing the Universal Soil Loss Equation with the following parameters:

1. Rainfall Factor, R 40
2. Soil Erodibility Factor, K 0.32
3. Slope Factor, LS 8.53
4. Cover Factor, C 0.794
5. Erosion Control Factor, P 1.0

The hydrologic analysis gives the storage volume required to contain the 10-year, 24-hour storm, and the remaining storage volume available for storing sediment. The existing storage capacity of J28-D is shown on Plate 3, Volume-Elevation Curve, J28-D, and the results of the analysis are summarized in the following table.

J28-D STORAGE

Total Storage Capacity	17.6	acre-ft
10-year, 24-hour Storm Inflow	2.79	acre-ft
Available Sediment Storage Capacity . .	14.77	acre-ft
Sediment Inflow Rate	1.22	acre-ft/yr
Sediment Storage Life	12	yrs

REMEDIAL COMPLIANCE PLAN

GEOTECHNICS

The inspection of Structure J28-D indicated that the only geotechnical problem is rill and gulley erosion on the upstream slope. Correction of erosion is considered a periodic maintenance task and does not require remedial action. The downstream slope should be flattened to 2.5 horizontal to 1 vertical to meet stability requirements.

HYDRAULICS

The storage capacity and spillway capacity of Structure J28-D are adequate; however, the spillway does not have an adequate outflow channel or adequate erosion protection. A trapezoidal outflow channel should be constructed along the alignment B-B' shown in Plate 1. The channel profile is shown in Plate 4 and the required dimensions are shown in Plate 5. Both the spillway and outflow channel should be protected against erosion using geotextile and gravel as shown in Plate 5.

* * *

The following plates and appendix are attached and complete this inspection report.

Plate 1 - Site Plan J28-D

Plate 2 - Existing Maximum Cross Section J28-D, A-A'

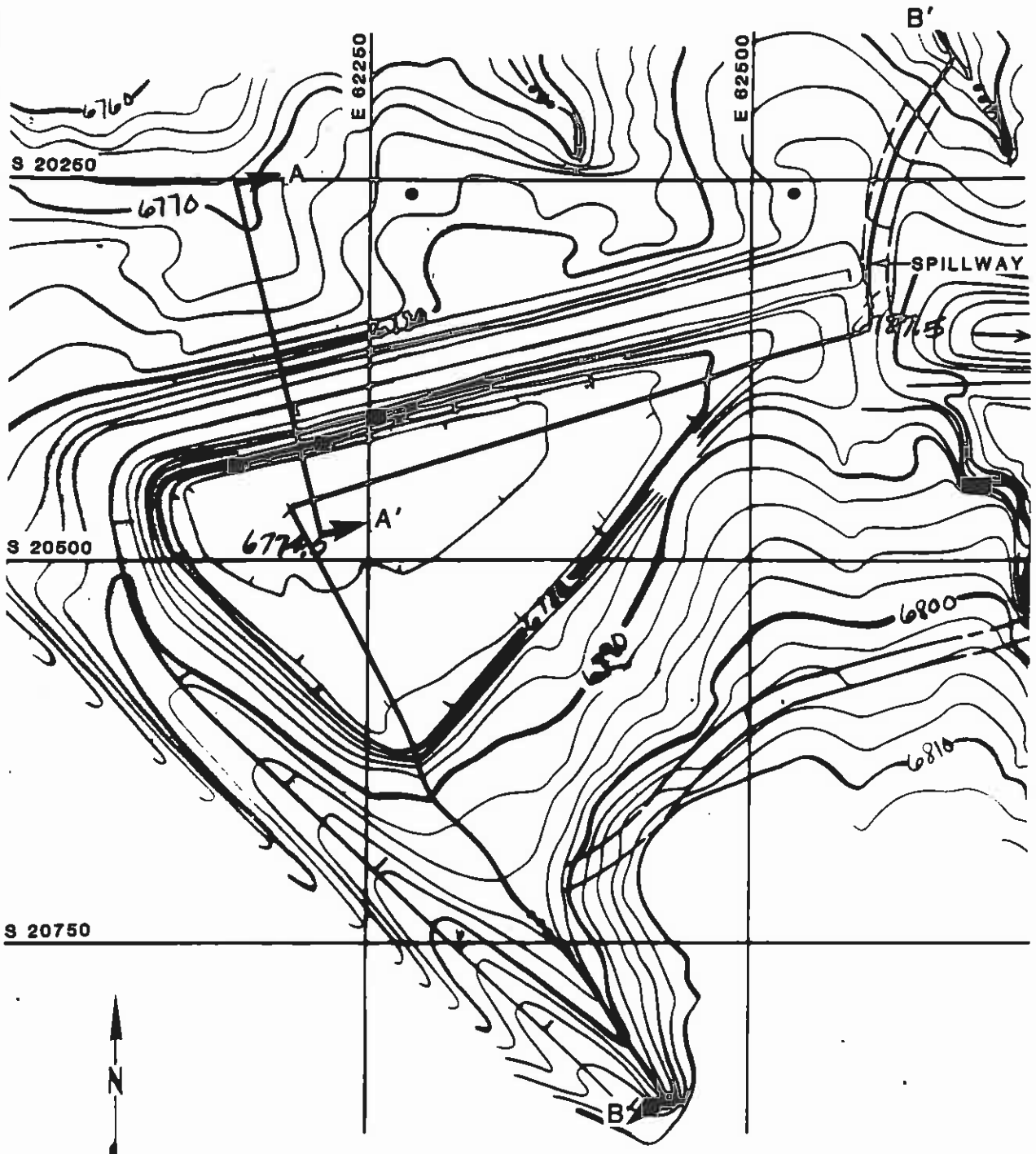
Plate 3 - Volume-Elevation Curve J28-D

Plate 4 - Channel Profile J28-D, B-B'

Plate 5 - Spillway and Outflow Channel Cross Section J28-D

Appendix A - Inspection Check List

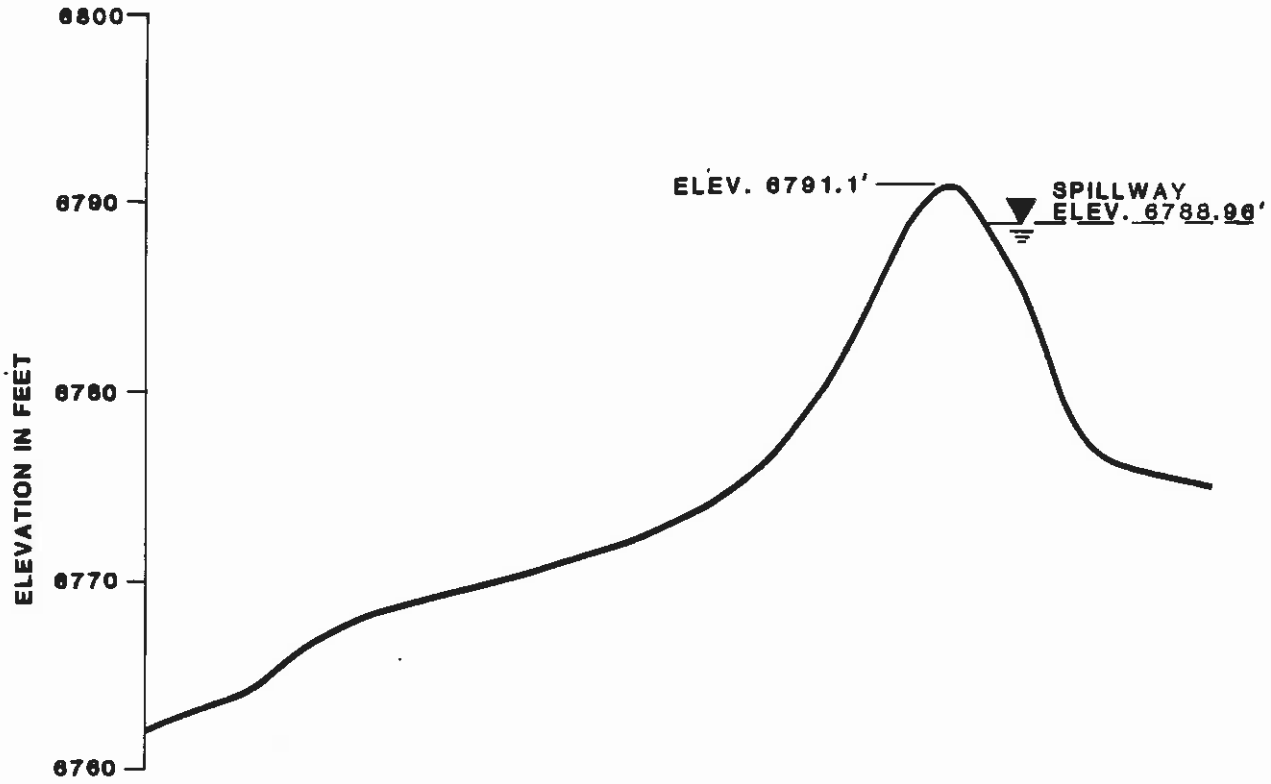
Appendix B - Hydrology and Hydraulic Calculations



SCALE
0 100 200
FEET

SITE PLAN
J28-D

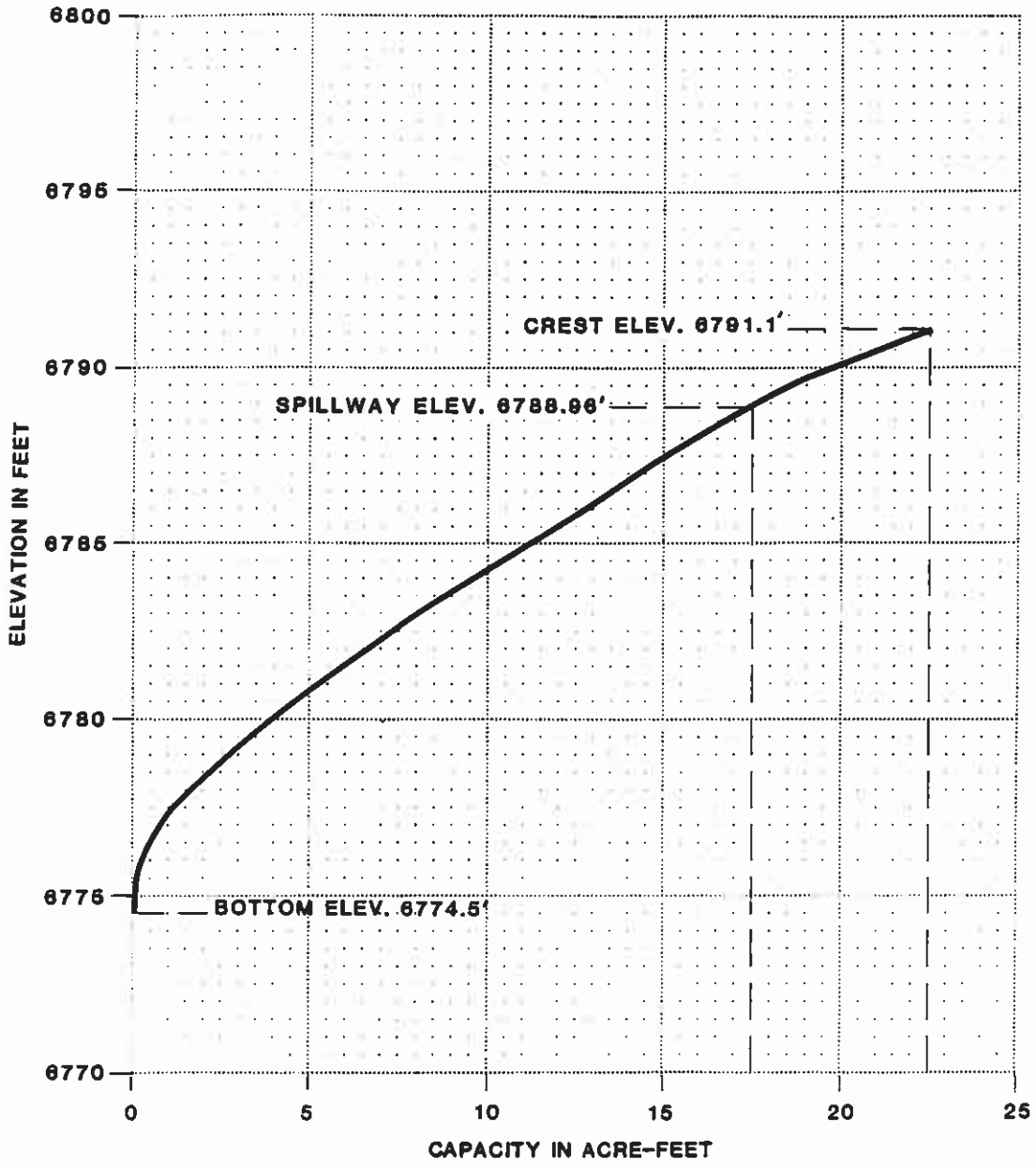
BY **Dames & Moore** Plate 1



SCALE
0 50 100
FEET

EXISTING MAXIMUM CROSS-SECTION A-A' J28-D

BY **Dames & Moore** Plate 2

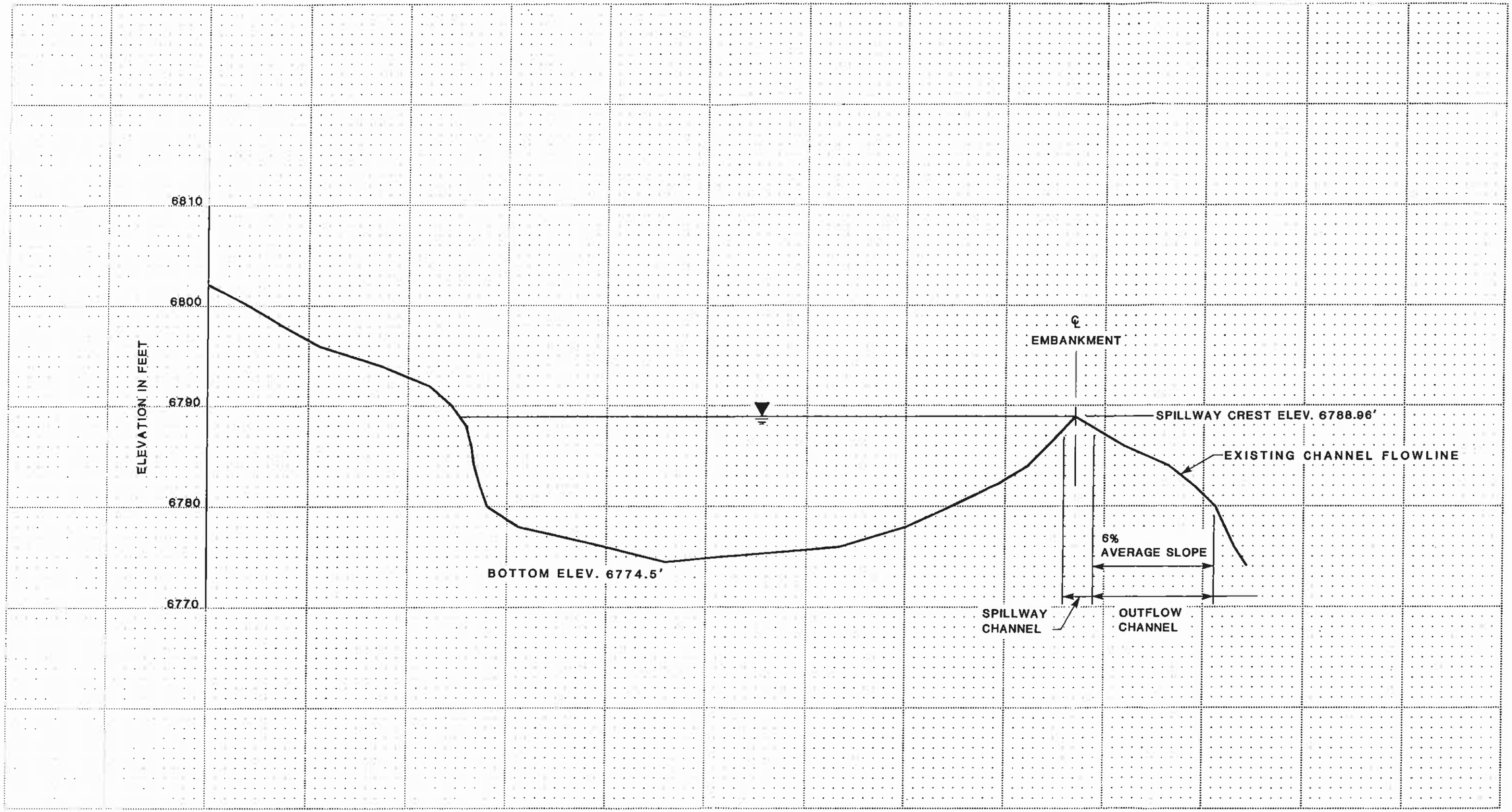


VOLUME-ELEVATION CURVE

J28-D

BY **Dames & Moore**

Plate 3

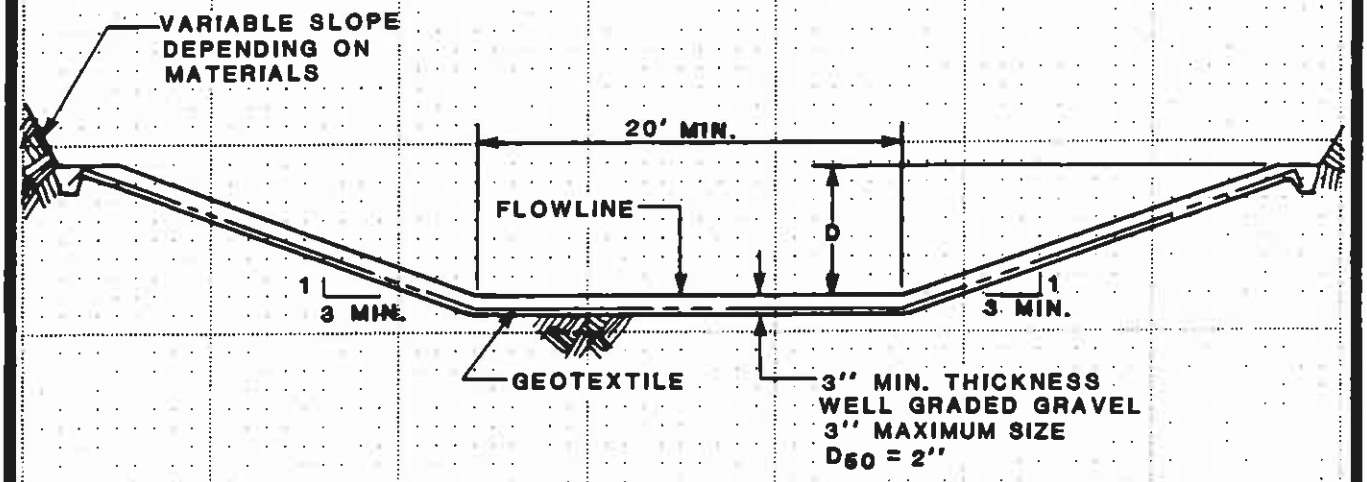


SCALE
0 100 200
FEET

CHANNEL PROFILE B–B'
J28–D

FOR LOCATION SEE PLATE 1

BY **Dames & Moore** Plate 4



SPILLWAY CHANNEL

D = 1.8'

LENGTH = 30'

FLOWLINE ELEV.= 6788.96'

OUTFLOW CHANNEL

D = 1'

SPILLWAY AND OUTFLOW CHANNEL CROSS SECTION J28-D

BY **Dames & Moore** Plate 5

APPENDIX A

INSPECTION CHECK LIST

Sediment Impoundment Name: J 28 - D
Page: 4

INSPECTION CHECK LIST

ITEM	YES	NO	REMARKS
1. CREST			15'w
a. Any visual settlements?		X	
b. Misalignment?		X	
c. Cracking?		X	
2. UPSTREAM SLOPE			32° on long leg of crest 21° on short leg.
a. Adequate grass cover?		X	
b. Any erosion?	X		Rills & one or two gullys
c. Are trees growing on slope?		X	
d. Longitudinal cracks?		X	
e. Transverse cracks?		X	
f. Adequate riprap protection?		X	
g. Any stone deterioration?			NA
h. Visual depressions or bulges?		X	
i. Visual settlements?		X	
j. Animal burrows?		X	
3. DOWNSTREAM SLOPE			23°
a. Adequate grass cover?	X		
b. Any erosion?		X	
c. Are trees growing on slope?		X	
d. Longitudinal cracks?		X	
e. Transverse cracks?		X	
f. Visual depressions or bulges?		X	
g. Visual settlements?		X	
h. Is the toe drain dry?			NA
i. Are the relief wells flowing?			NA
j. Are boils present at the toe?		X	
k. Is seepage present?		X	
l. Animal burrows?		X	
4. ABUTMENT CONTACT. RIGHT			
a. Any erosion?		X	
b. Visual differential movement?		X	
c. Any cracks noted?		X	
d. Is seepage present?		X	
e. Type of Material?			brown SM
5. ABUTMENT CONTACT. LEFT			
a. Any erosion?		X	
b. Visual differential movement?		X	
c. Any cracks noted?		X	
d. Is seepage present?		X	
e. Type of Material?			brown SM

ITEM	YES	NO	REMARKS
6. SPILLWAY/NORMAL			
a. Location:			
Left abutment?			
Right abutment?	X		
Crest of Embankments?			
b. Approach Channel:		X	
Are side slopes eroding?			
Are side slopes sloughing?			
Bottom of channel eroding?			NA
Obstructed?			
Erosion protection?			
c. Spillway Channel:	X		17'W 25'L 0% Slope 3.0' below crest
Are side slopes eroding?		X	
Are side slopes sloughing?		X	
Bottom of channel eroding?		X	
Obstructed?		X	
Erosion protection?		X	
d. Outflow Channel:	X		17'W ± 120' 2% Slope
Are side slopes eroding?		X	
Are side slopes sloughing?		X	
Bottom of channel eroding?		X	
Obstructed?	X		Fence across channel, may catch brush & slow flow
Erosion protection?		X	
e. Weir:		X	
Condition?			
7. SPILLWAY/EMERGENCY			NA
a. Location:			
Left abutment?			
Right abutment?			
Crest of Embankments?			
b. Approach Channel:			
Are side slopes eroding?			
Are side slopes sloughing?			
Bottom of channel eroding?			
Obstructed?			
Erosion protection?			
c. Spillway Channel:			
Are side slopes eroding?			
Are side slopes sloughing?			
Bottom of channel eroding?			
Obstructed?			
Erosion protection?			
d. Outflow Channel:			
Are side slopes eroding?			
Are side slopes sloughing?			
Bottom of channel eroding?			
Obstructed?			
Erosion protection?			
e. Weir:			
Condition?			

ITEM	YES	NO	REMARKS
8. IMPOUNDMENT			
a. Sinkholes?		X	(Elev.) feet
b. Water present?	X		(Elev.) feet
c. Siltation?	X		
d. Watershed matches soil map?		X	

9. GENERAL COMMENTS

Canopy 0 %
Ground 35 %

APPENDIX B

HYDROLOGY AND HYDRAULIC CALCULATIONS

FILE PEABODY COAL CO 10134-011-22
SUBJECT SEDIMENT POND HYDROLOGY
J28-D SHEET ___ OF ___

REVISIONS
BY ___ DATE ___ TO EO ___
BY ___ DATE ___ TO EO ___

TIME OF CONCENTRATION

ELEVATION DIFFERENCE = 6895 − 6789 = 106 ft.

WATER COURSE LENGTH = 3.0(400) = 1200 ft. = 0.227 mi.

$$T_c = \left(\frac{11.9\ (0.227)^3}{106}\right)^{0.385} = 0.078 \text{ hr.}$$

LAG TIME = $0.6\,T_c$ = 0.047 hr.

SCS CURVE NUMBER

DRAINAGE AREA (ac)	COVER TYPE	HYDROLOGIC CONDITION	SOIL TYPE	WEIGHTED CURVE NUMBER
7.3	P-J	average	C	78 (.24)
23.1	disturbed	—	C	91 (.76)
				87.9

100% EH #26

use 88

DRAINAGE BASIN AREA

30.4 ACRE 0.048 SQ MILE

BY S. DOLAN DATE 10-2-85
CHECKED BY ___
COPY TO EO ___

FILE HEADLEY COAL CO 10139-01-22
SUBJECT SEDIMENT INFLOW
J28-D SHEET ___ OF ___

REVISIONS
BY ___ DATE ___ TO EO ___
BY ___ DATE ___ TO EO ___

UNIVERSAL SOIL LOSS EQUATION

RAINFALL FACTOR

K= 40

SOIL ERODIBILITY FACTOR

SOIL TYPE = 100% EH #26 = .32

K = .32

SLOPE FACTOR

LENGTH (ft)	Δ ELEV (ft)	SLOPE (%)	LS
600	130	21.7	11.4 (.7)
500	35	7.0	1.84 (.3)
			= 8.53

COVER FACTOR

AREA (ac)	COVER TYPE	% COVER	CANOPY (%)	WEIGHTED C
24 %	P-J	40	25	.24(.14)
76 %	disturbed	—	—	.76(1.0)
				C= .794

EROSION CONTROL FACTOR

P= 1.0

SEDIMENT INFLOW

BY ___ DATE ___
CHECKED BY ___
COPY TO EO ___

$A = 40(.32)(8.53)(.794)(1.0) = 86.69$ ton/acre/year

$A = (86.69)\left(\frac{1}{2047}\right)(30.4)(.95) = 1.22$ acre-feet/year

Dames & Moore