

DESIGN REPORT
Permanent Impoundment Structure
J27-RA
Black Mesa Mine
Navajo County, Arizona

for
PEABODY WESTERN COAL COMPANY

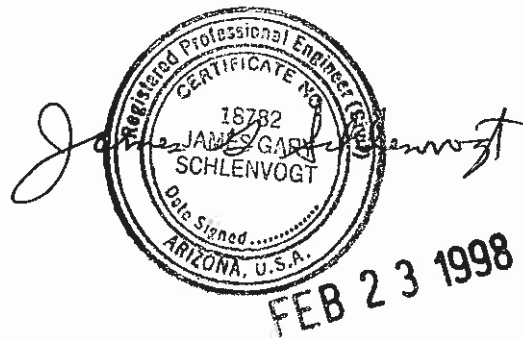


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INTRODUCTION

Structure J27-RA is an existing earthen embankment structure constructed by Peabody Western Coal Company in the J-27 reclamation area and proposed as a permanent structure to impound a maximum of approximately 2.63 ac.-ft. of runoff from the adjacent reclaimed areas of the Black Mesa Mine. The location of structure J27-RA and its watershed boundary are shown on Drawing No. 85400 (Sheet L-10) and Drawing No. 85405. The existing structure and the site-specific general construction plans addressing the existing embankment configuration and spillway designs are shown on the attached Exhibit 1.

This design report contains information specific to structure J27-RA, which is in series with Structure J27-RC. Mine-wide design, construction, and reclamation information is presented in the "General Report, Kayenta and Black Mesa Mines, Navajo County, Arizona for Peabody Western Coal Company", December, 1985 (PAP), Chapter 6, Attachment D, Volume 2, along with the methods and results of analyses used for slope stability, hydrology, and hydraulics, and in Chapter 6, Pages 11 to 42, "Sediment and Water Control Facility Plan".

INSPECTION

The construction site of the existing structure J27-RA was inspected by a Registered Professional Engineer from Peabody Western Coal Company, to assure that the existing structure is stable and no adverse conditions existed to prevent successful construction of the spillway structure. A detailed geotechnical investigation was not performed; rather, the information in Chapter 6, Attachment D was utilized to evaluate embankment design.

SITE DESCRIPTION

LAND USE

The J27-RA structure has a 45.8-acre tributary drainage area and is located on a tributary to Moenkopi Wash. The 45.8 acre watershed contributing to the J27-RA structure is classified as 19% Post-Law reclaimed and 81% Pre-Law reclaimed.

DESIGN ANALYSES

GENERAL

Structure J27-RA was designed under the supervision of a Registered Professional Engineer from Peabody Western Coal Company. The design was performed in accordance with applicable 30 CFR 780 and 816 regulations of the United States Department of Interior, Office of Surface Mining (OSM) and included a review of available project files. The most current information contained in the Peabody Western Coal Company files includes topographic maps developed from aerial photography flown in 1997 for Peabody Western Coal Company and was used in the analysis of the structure.

STABILITY

Structure J27-RA is conservatively assumed to be a Category A-5 embankment. A homogeneous earthen embankment approximately 15 feet wide on top currently exists. The upstream slope will be constructed to 2.5:1 (horizontal to vertical) or flatter slope and the downstream slope will be constructed to 3.5:1 or flatter slope. Based on the total embankment height of approximately 13 feet, these slopes are equal to or flatter than the recommended "worst case" embankment/foundation condition slopes in Table 3-6, Attachment D, Chapter 6; therefore, the embankment will be stable. The emergency spillway will be a minimum 10-foot wide riprap-lined trapezoidal channel.

WATER PERSISTENCE

Pond J27-RA is a relatively small pond with an adequate contributing drainage area. As a result, there is standing water in the pond over a significant portion of the year with an average depth ranging from 3 to 7 feet. Both PWCC personnel and the OSM Inspectors have observed water occurrence in the pond over a period of several years.

In addition, to determine water persistence for Structure J27-RA, runoff from average annual precipitation was compared to evaporation and infiltration rates on a monthly basis. Initially, the pond was assumed to be empty. Runoff for the first month was determined using the SCS Curve Number Method and the mean monthly precipitation for January, as presented in Appendices C and described in subsequent sections. The runoff volume was added to the pond and a water elevation and surface area were determined from the pond stage storage curve found on Appendix C. Once the water surface area was determined, the total evaporation and infiltration for the first month were calculated. The calculated evaporation and infiltration losses were subtracted from the total runoff for the first month to determine the average water increase or decrease to the pond. The final volume was then used as the starting volume for the next month and the same steps were repeated for each subsequent month. This analysis proceeded until the pond elevation and surface area stabilized, which occurred in year 2. The inputs and results are shown in Appendix C in both graphical and tabular formats. As shown by the graph and table in Appendix C, the water elevation of the

pond should stabilize between elevation 6539.5 and the spillway invert, depending on the time of year. This is the point at which runoff rates equal the evaporation and infiltration rates and or runoff discharges through the spillway and corresponds to approximately 1.5 to 2.6 ac-ft of water in the impoundment. In 1982 and 1983, Water, Waste and Land (WWL), Consultants, also prepared a study for PWCC and OSM which is included in Volume 27, Appendix E. They evaluated and determined these types of impoundments located in areas reclaimed in the late 1970's and early 1980's were stable.

WATER QUALITY

Water in the J27-RA Permanent Impoundment comes primarily from surface water runoff from the J27 reclamation area. Given that the spoils in the J27 area do not contain material which is potentially acid- or toxic-forming and could adversely impact surface runoff water quality, Peabody Western Coal Company does not anticipate any significant water quality problems. The structure has been containing water for many years and no adverse condition from the water has been noted in the wildlife or domestic animals observed in the area.

HYDROLOGY

The hydrologic analysis was completed using the computer program SEDCAD+ (see Appendices A, and B). Structure J27-RA is constructed in series with downstream Structure J27-RC. Structure J27-RA is classified as a low hazard structure (see Drawing No. 85408). The mine area is sparsely populated with no one living in the downstream floodplain. The structure will impound less than 20 acre-feet and is less than 20 vertical feet in height from the upstream toe of embankment of the natural stream elevation to the emergency spillway invert elevation. The structure is located upstream of Structure J27-RC; and although the cumulative capacity of these impoundments is less than 20 acre-feet, the spillway was analyzed using the 100-year, 6-hour storm event given the potential for flow between structures. Structure J27-RA was conservatively assumed to be full to the invert of the emergency spillway at the time of 100-year storm event.

The following parameters were used in the hydrologic analysis for the 100-yr., 6-hr storm (see Appendix B):

J27-RA

1. Water Course length, L 0.456 mi.
2. Elevation Difference, H 142 ft
3. Time of Concentration, T_c 0.156 hr
4. SCS Curve Number 86
5. Rainfall Depth, 100-year, 6-hour storm 2.4 in
6. Drainage Area 45.8 acres

HYDRAULICS

The SEDCAD+ and Flow Master computer programs were used to evaluate inflow to the sedimentation structure, outflow from the structure and the resulting water surface elevations. The initial conditions and results of the analysis are summarized in the following table (supporting calculations are presented in Appendices A, and B).

J27-RA SEDIMENTATION POND HYDRAULICS TABLE

| | <u>Units</u> | <u>100-Yr., 6-Hr</u> <u>Storm</u> |
|------------------------------------|--------------|--------------------------------------|
| Initial Reservoir Volume Condition | | Full to emergency spillway |
| Inflow | | |
| Peak Flow | cfs | 73.7 |
| Volume | ac-ft | 4.4 |
| Outflow | | |
| Peak Flow | cfs | 59.7 |
| Spillway Elevation | msl | 6541.0 |
| Embankment Crest Elev. | msl | 6544.0 |
| Peak Stage | msl | 6542.6 |
| Freeboard | ft | 1.4 |
| Emergency Spillway Channel | | |
| Flow Depth | ft | 1.6 |
| Critical Velocity | fps | 5.0 |
| Mannings "n" | -- | .035 |
| Width | ft | 10 |
| Outflow Channel | | |
| Maximum Slope | % | 16.7 |
| Normal Velocity | fps | 7.4 |
| Normal Depth | ft | 0.7 |
| Mannings "n" | -- | .057 |
| Riprap D ₅₀ | in | 6 |

EMERGENCY SPILLWAY AND OUTLET CHANNEL

The emergency spillway and outlet channel for J27-RA will be a trapezoidal channel, the alignment and dimensions are shown on Exhibit 1 and includes the following dimensions:

| | | | |
|-------------------------------------|------------|--------|------------|
| Minimum Channel Depth | (Spillway) | 3.0 | ft |
| | (Outflow) | 1.7 | ft |
| Channel Width | | 10 | ft |
| Channel Length | (Spillway) | 40 | ft |
| | (Outflow) | 125 | ft |
| Sideslopes (Horizontal to Vertical) | | 3:1 | or flatter |
| Average Slope | (Spillway) | 0.0 | % |
| Maximum Slope | (Outflow) | 16.7 | % |
| Spillway Elevation | | 6541.0 | ft |

A minimum 15-foot long riprap lined channel will be constructed beyond the toe of the embankment as a transition into the downstream natural channel.

STORAGE CAPACITY

The impoundment stage-capacity table (see Exhibit 1) is based on the 1997 aerial topography mapping conducted for Peabody Western Coal Company. Structure J27-RA is designed to contain approximately 2.63 acre-feet.

The calculations for the sediment load entering structure J27-RA were made utilizing the Revised Universal Soil Loss Equation with the following input parameters:

| | | |
|----|----------------------------|------|
| 1. | Rainfall Factor, R | 40 |
| 2. | Soil Erodibility Factor, K | 0.38 |
| 3. | Slope Factor, LS | 1.88 |
| 4. | Cover Factor, C | 0.22 |
| 5. | Erosion Control Factor, P | 1.00 |

To determine the potential life of the structure, the results of the sediment storage capacity for the J27-RA pond are presented in the following table.

J27-RA STORAGE

| | | |
|----------------------------------|------|----------------|
| Total Available Storage Capacity | 2.63 | acre-feet |
| Sediment Inflow Rate/Year | 0.13 | acre-feet/year |
| Sediment Storage Life | 20 | years |

The following appendices and drawing are attached and complete this design report.

- Appendix A - Hydrology, Hydraulic, and Sedimentation Calculations
- Appendix B - SEDCAD+ (Input and Output) 100-Year, 6-Hour Storm Event
- Appendix C -Water Persistence Calculations
- Exhibit #1 - J27-RA Permanent Impoundment Design

APPENDIX A

Hydrology, Hydraulic, and Sedimentation Calculations

I::

PEABODY WESTERN COAL COMPANY
CALCULATED HYDROLOGIC DATA

PROJECT: J27 AREA

STRUCTURE: J27-RA

TIME OF CONCENTRATION:

Start Elevation (ft) = 6680
End Elevation (ft) = 6538
Elevation Difference, E (ft) = 142

Watercourse Length (ft) = 2410
Watercourse Length, L (mi) = 0.456

 $T_c = (11.9L^3/E)^{0.385} = \underline{\underline{0.156}}$

ROUTING PARAMETERS:

Between structure routing parameters were calculated using the SCS Upland Method in SEDCAD+. Input and output parameters are shown on the SEDCAD+ printouts in Appendices B and C.

SCS CURVE NUMBER:

| Cover Type | Soil Group | Curve Number | Area (acres) | CN*Area |
|--------------------|------------|--------------|--------------|---------|
| Pre-Law Reclaimed | C | 87 | 37.1 | 3227.7 |
| Post-Law Reclaimed | C | 81 | 8.7 | 704.7 |
| TOTAL: | | | 45.8 | 3932.4 |

Weighted CN = Total CN*Area/ Total Area = 86

DRAINAGE BASIN AREA:

45.8 Acres

**PEABODY WESTERN COAL COMPANY
CALCULATED SEDIMENTOLOGY DATA**

PROJECT: J27 AREA

STRUCTURE: J27-RA

SOIL ERODIBILITY FACTOR:

| Soil Type | Erodibility Factor, K | Area (acres) | K*Area |
|-----------|--------------------------|-----------------|--------|
| EH#35 | 0.38 | 45.8 | 17.40 |
| TOTAL: | | 45.8 | 17.40 |

Weighted K = Total K*Area/ Total Area = 0.38

SLOPE FACTOR:

| Length (ft) | Elevation Change (ft) | Slope (%) | m | Slope Angle (deg) | LS Factor |
|----------------|-----------------------------|--------------|-----|-------------------------|--------------|
| 300 | 20 | 6.7% | 0.5 | 3.8 | 1.52 |
| 100 | 20 | 20.0% | 0.6 | 11.3 | 3.39 |
| 150 | 20 | 13.3% | 0.6 | 7.6 | 2.66 |
| 340 | 30 | 8.8% | 0.5 | 5.0 | 2.12 |
| 200 | 15 | 7.5% | 0.5 | 4.3 | 1.39 |
| 250 | 10 | 4.0% | 0.4 | 2.3 | 0.76 |
| 400 | 20 | 5.0% | 0.5 | 2.9 | 1.34 |

Average LS = 1.88

The LS Factor was calculated by:

$LS = (Slope\ Length / 72.6)^m * (10.8 * \sin(slope\ angle) + 0.03)$ for Slopes < 9%

$LS = (Slope\ Length / 72.6)^m * (16.8 * \sin(slope\ angle) - 0.5)$ for Slopes > 9%

Where:

Slope < 3% $m = 0.3$
 Slope = 4% $m = 0.4$
 5% > Slope < 10% $m = 0.5$
 Slope > 10% $m = 0.6$

l::

COVER AND PRACTICE FACTORS:

| Cover Type | Cover (%) | Canopy (%) | Area (acres) | Cover Factor, C | C*Area | Practice Factor, P | P*Area |
|------------|-----------|------------|--------------|-----------------|--------|--------------------|--------|
| Pre Law | 20% | 0% | 37.1 | 0.24 | 8.90 | 1.00 | 37.10 |
| Post Law | 40% | 0% | 8.7 | 0.15 | 1.31 | 1.00 | 8.70 |
| TOTAL: | | | 45.8 | | 10.21 | | 45.80 |

Weighted C = Total C*Area/ Total Area = 0.223

Weighted P = Total P*Area/ Total Area = 1.000

RAINFALL FACTOR:

R = 40

PEABODY WESTERN COAL COMPANY
CALCULATED SEDIMENT YIELD

PROJECT: J27 AREA

STRUCTURE: J27-RA

The following spreadsheet calculates the predicted sediment yield for the project area. The gross sediment yield is determined according to the Revised Universal Soil Loss Equation.

| PARAMETER DESCRIPTION | VALUE |
|---------------------------------|----------------------------|
| Annual Rainfall Factor | 40.00 |
| Soil Erodibility Factor | 0.38 |
| Length Slope Factor | 1.88 |
| Cover Factor | 0.22 |
| Practice Factor | 1.00 |
| Gross Annual Sediment Yield | 6.37 tons/acre/year |
| Sediment Density | 94.00 pcf |
| Gross Annual Sediment Yield | 0.0031 acre-feet/acre/year |
| Sediment Delivery Ratio | 90% |
| Estimated Annual Sediment Yield | 0.0028 acre-feet/acre/year |
| Watershed Area | 45.8 acres |
| Watershed Annual Sediment Yield | 0.13 acre-feet/year |
| Number of years | 1 years |
| Calculated Sediment Volume | 0.13 acre-feet |

SEDCAD+ RIPRAP CHANNEL DESIGN

J27-RA OUTFLOW CHANNEL

INPUT VALUES:

| | | |
|----------------------|-------------|--------|
| Shape | TRAPEZOIDAL | |
| Discharge | 59.70 cfs | |
| Slope | 16.70 % | |
| Sideslopes (L and R) | 3.00:1 | 3.00:1 |
| Bottom Width | 10.00 feet | |
| Freeboard | None | |

RESULTS:

Steep Slope Design - PADER Method

| | |
|----------------------|---------------------|
| Depth | 0.68 ft |
| with Freeboard | 0.00 ft |
| Top Width | 14.06 ft |
| with Freeboard | 10.00 ft |
| Velocity | 7.34 fps |
| Cross Sectional Area | 8.13 sq ft |
| Hydraulic Radius | 0.57 ft |
| Manning's n | 0.057 |
| Froude Number | 1.70 |
| Dmax | 0.625 ft (7.50 in) |
| D50 | 0.500 ft (6.00 in) |
| D10 | 0.167 ft (2.00 in) |

J27-RA Spillway
Worksheet for Trapezoidal Channel

| Project Description | |
|---------------------|---------------------|
| Project File | untitled.fm2 |
| Worksheet | J27-RA Spillway |
| Flow Element | Trapezoidal Channel |
| Method | Manning's Formula |
| Solve For | Channel Depth |

| Input Data | | |
|----------------------|----------------|-----|
| Mannings Coefficient | 0.035 | |
| Channel Slope | 0.019996 ft/ft | |
| Left Side Slope | 3.000000 H : V | |
| Right Side Slope | 3.000000 H : V | |
| Bottom Width | 10.00 | ft |
| Discharge | 59.70 | cfs |

| Results | | |
|------------------------|----------------|-----------------|
| Depth | 0.94 | ft |
| Flow Area | 12.01 | ft ² |
| Wetted Perimeter | 15.93 | ft |
| Top Width | 15.62 | ft |
| Critical Depth | 0.94 | ft |
| Critical Slope | 0.019996 ft/ft | |
| Velocity | 4.97 | ft/s |
| Velocity Head | 0.38 | ft |
| Specific Energy | 1.32 | ft |
| Froude Number | 1.00 | |
| Flow is supercritical. | | |

APPENDIX B

SEDCAD+ (Input and Output) 100-Year, 6-Hour Storm Event

CIVIL SOFTWARE DESIGN

SEDCAD+ Version 3

J-27 AREA

by

Name: D. GLEASON

Company Name: ACZ, INC.
File Name: J:\861\0500\J-27-2II

Date: 12-12-1997

Company Name: ACZ, INC.

Filename: J:\861\0500\J-27-2II User: D. GLEASON

Date: 12-12-1997 Time: 13:46:21

J-27 AREA

Storm: 2.40 inches, 100 year- 6 hour, SCS Type II

Hydrograph Convolution Interval: 0.1 hr

=====

GENERAL INPUT TABLE

=====

Detailed Between Structure Routing:

| J | B | To | Seg. | Land Flow Condition | Distance (ft) | Slope (%) | Velocity (fps) | Segment Time (hr) | Muskingum | |
|---|---|----|------|------------------------|------------------|--------------|-------------------|-------------------------|-----------|-------|
| | | S | # | | | | | | K (hr) | X |
| 1 | 1 | 2 | 1 | 8 | 705.15 | 8.57 | 8.78 | 0.02 | 0.022 | 0.418 |
| 1 | 2 | 2 | 1 | 8 | 1304.92 | 6.15 | 7.44 | 0.05 | 0.048 | 0.406 |
| 2 | 1 | 1 | 1 | 8 | 52.00 | 20.00 | 13.42 | 0.00 | 0.001 | 0.443 |

Company Name: ACZ, INC.
 Filename: J:\861\0500\J-27-2II User: D. GLEASON
 Date: 12-12-1997 Time: 13:46:21
 J-27 AREA
 Storm: 2.40 inches, 100 year- 6 hour, SCS Type II
 Hydrograph Convolution Interval: 0.1 hr

=====

SUBWATERSHED/STRUCTURE INPUT/OUTPUT TABLE

=====

-Hydrology-

| JBS | SWS | Area (ac) | CN | UHS | Tc (hrs) | K (hrs) | X | Base- Flow (cfs) | Runoff Volume (ac-ft) | Peak Discharge (cfs) |
|--------------------|--------------|--------------|------------|-----|---------------|------------|-------|------------------------|-----------------------------|----------------------------|
| 111 | 1 | 45.80 | 86 | F | 0.156 | 0.000 | 0.000 | 0.0 | 4.44 | 73.66 |
| | | | Type: Pond | | Label: J27-RA | | | | | |
| 111 | Structure | 45.80 | | | | | | | 4.44 | |
| 111 | Total IN | 45.80 | | | | | | | 4.44 | 73.66 |
| 111 | Total OUT | | | | | | | | 4.44 | 59.70 |
| 112 | 1 | 31.10 | 84 | F | 0.182 | 0.000 | 0.000 | 0.0 | 2.69 | 44.08 |
| | | | Type: Null | | Label: NULL 1 | | | | | |
| | Structure | 31.10 | | | | | | | 7.13 | |
| 112 | Total IN/OUT | 76.90 | | | | | | | 7.13 | 103.07 |
| 111 to 112 Routing | | | | | | 0.022 | 0.418 | | | |
| 121 | 1 | 10.80 | 84 | F | 0.078 | 0.000 | 0.000 | 0.0 | 0.94 | 17.78 |
| | | | Type: Pond | | Label: J27-RB | | | | | |
| 121 | Structure | 10.80 | | | | | | | 0.94 | |
| 121 | Total IN | 10.80 | | | | | | | 0.94 | 17.78 |
| 121 | Total OUT | | | | | | | | 0.94 | 10.35 |
| 122 | 1 | 40.90 | 85 | F | 0.098 | 0.000 | 0.000 | 0.0 | 3.75 | 70.35 |
| | | | Type: Null | | Label: NULL 2 | | | | | |
| 122 | Structure | 40.90 | | | | | | | 4.68 | |
| 122 | Total IN/OUT | 51.70 | | | | | | | 4.68 | 80.59 |
| 121 to 122 Routing | | | | | | 0.048 | 0.407 | | | |
| 211 | 1 | 14.80 | 85 | F | 0.095 | 0.000 | 0.000 | 0.0 | 1.36 | 25.46 |
| | | | Type: Pond | | Label: J27-RC | | | | | |
| 211 | Structure | 14.80 | | | | | | | 13.17 | |
| | Total IN | 143.40 | | | | | | | 13.17 | 188.24 |
| | Total OUT | | | | | | | | 13.17 | 158.90 |
| 112 to 211 Routing | | | | | | 0.001 | 0.443 | | | |

Company Name: ACZ, INC.

Filename: J:\861\0500\J-27-2II User: D. GLEASON

Date: 12-12-1997 Time: 13:46:21

J-27 AREA

Storm: 2.40 inches, 100 year- 6 hour, SCS Type II

Hydrograph Convolution Interval: 0.1 hr

=====

POND INPUT/OUTPUT TABLE

=====

J1, B1, S1
J27-RA

Drainage Area from J1, B1, S1, SWS(s)1: 45.8 acres
Total Contributing Drainage Area: 45.8 acres

DISCHARGE OPTIONS:

Emergency
Spillway

=====

| | |
|----------------------|------|
| Riser Diameter (in) | ---- |
| Riser Height (ft) | ---- |
| Barrel Diameter (in) | ---- |
| Barrel Length (ft) | ---- |
| Barrel Slope (%) | ---- |
| Manning's n of Pipe | ---- |
| Spillway Elevation | ---- |

| | |
|---------------------------|------|
| Lowest Elevation of Holes | ---- |
| # of Holes/Elevation | ---- |

| | |
|---------------------------|------|
| Entrance Loss Coefficient | ---- |
| Tailwater Depth (ft) | ---- |

| | |
|-----------------------|------|
| Notch Angle (degrees) | ---- |
| Weir Width (ft) | ---- |

| | |
|---------------------------|------|
| Siphon Crest Elevation | ---- |
| Siphon Tube Diameter (in) | ---- |
| Siphon Tube Length (ft) | ---- |
| Manning's n of Siphon | ---- |
| Siphon Inlet Elevation | ---- |
| Siphon Outlet Elevation | ---- |

| | |
|------------------------------|--------|
| Emergency Spillway Elevation | 6541.0 |
| Crest Length (ft) | 40.0 |
| Z:1 (Left and Right) | 3 3 |
| Bottom Width (ft) | 10.0 |

D RESULTS:

Permanent
Pool
(ac-ft)

=====

2.6

| | Runoff Volume (ac-ft) | Peak Discharge (cfs) |
|-----|-----------------------------|----------------------------|
| IN | 4.44 | 73.66 |
| OUT | 4.44 | 59.70 |

| Peak Elevation | Hydrograph Detention Time (hrs) |
|-------------------|---------------------------------------|
| 6542.6 | 0.20 |

J1, B2, S1
J27-RB

| | |
|---|------------|
| Drainage Area from J1, B2, S1, SWS(s)1: | 10.8 acres |
| Total Contributing Drainage Area: | 10.8 acres |

DISCHARGE OPTIONS:

| | Emergency Spillway |
|------------------------------|-----------------------|
| Riser Diameter (in) | ---- |
| Riser Height (ft) | ---- |
| Barrel Diameter (in) | ---- |
| Barrel Length (ft) | ---- |
| Barrel Slope (%) | ---- |
| Manning's n of Pipe | ---- |
| Spillway Elevation | ---- |
| Lowest Elevation of Holes | ---- |
| # of Holes/Elevation | ---- |
| Entrance Loss Coefficient | ---- |
| Tailwater Depth (ft) | ---- |
| Notch Angle (degrees) | ---- |
| Weir Width (ft) | ---- |
| Siphon Crest Elevation | ---- |
| Siphon Tube Diameter (in) | ---- |
| Siphon Tube Length (ft) | ---- |
| Manning's n of Siphon | ---- |
| Siphon Inlet Elevation | ---- |
| Siphon Outlet Elevation | ---- |
| Emergency Spillway Elevation | 6562.0 |
| Crest Length (ft) | 40.0 |
| Z:1 (Left and Right) | 3 3 |
| Bottom Width (ft) | 10.0 |

POND RESULTS:

Permanent
Pool
(ac-ft)

=====

1.4

| | Runoff Volume (ac-ft) | Peak Discharge (cfs) |
|-----|-----------------------------|----------------------------|
| IN | 0.94 | 17.78 |
| OUT | 0.94 | 10.35 |

| Peak Elevation | Hydrograph Detention Time (hrs) |
|-------------------|---------------------------------------|
| 6562.7 | 0.00 |

J2, B1, S1
J27-RC

| | |
|---|-------------|
| Drainage Area from J2, B1, S1, SWS(s)1: | 14.8 acres |
| Total Contributing Drainage Area: | 143.4 acres |

DISCHARGE OPTIONS:

Emergency
Spillway

| | |
|------------------------------|--------|
| er Diameter (in) | ---- |
| user Height (ft) | ---- |
| barrel Diameter (in) | ---- |
| Barrel Length (ft) | ---- |
| Barrel Slope (%) | ---- |
| Manning's n of Pipe | ---- |
| Spillway Elevation | ---- |
| Lowest Elevation of Holes | ---- |
| # of Holes/Elevation | ---- |
| Entrance Loss Coefficient | ---- |
| Tailwater Depth (ft) | ---- |
| Notch Angle (degrees) | ---- |
| Weir Width (ft) | ---- |
| Siphon Crest Elevation | ---- |
| Siphon Tube Diameter (in) | ---- |
| Siphon Tube Length (ft) | ---- |
| Manning's n of Siphon | ---- |
| Siphon Inlet Elevation | ---- |
| Siphon Outlet Elevation | ---- |
| Emergency Spillway Elevation | 6467.0 |
| st Length (ft) | 40.0 |
| (Left and Right) | 3 3 |
| Bottom Width (ft) | 20.0 |

POND RESULTS:

Permanent

Pool
(ac-ft)
=====

2.1

| | Runoff Volume (ac-ft) | Peak Discharge (cfs) |
|--|-----------------------------|----------------------------|
|--|-----------------------------|----------------------------|

| | | |
|-----|-------|--------|
| IN | 13.17 | 188.24 |
| OUT | 13.17 | 158.90 |

| Peak Elevation | Hydrograph Detention Time (hrs) |
|-------------------|---------------------------------------|
|-------------------|---------------------------------------|

| | |
|--------|------|
| 6469.0 | 0.17 |
|--------|------|

Company Name: ACZ, INC.

Filename: J:\861\0500\J-27-2II User: D. GLEASON

Date: 12-12-1997 Time: 13:46:21

J-27 AREA

Storm: 2.40 inches, 100 year- 6 hour, SCS Type II
Hydrograph Convolution Interval: 0.1 hr

=====

ELEVATION-AREA-CAPACITY-DISCHARGE TABLE

=====

J1, B1, S1
J27-RA

Drainage Area from J1, B1, S1, SWS(s)1: 45.8 acres
Total Contributing Drainage Area: 45.8 acres

SW#1: Emergency Spillway

| Elev | Stage (ft) | Area (ac) | Capacity (ac-ft) | Discharge (cfs) | |
|---------|---------------|--------------|---------------------|--------------------|---------------|
| 6532.00 | 0.00 | 0.01 | 0.00 | 0.00 | |
| 6533.00 | 1.00 | 0.07 | 0.04 | 0.00 | |
| 6534.00 | 2.00 | 0.17 | 0.16 | 0.00 | |
| 6535.00 | 3.00 | 0.22 | 0.36 | 0.00 | |
| 6536.00 | 4.00 | 0.27 | 0.61 | 0.00 | |
| 6537.00 | 5.00 | 0.32 | 0.91 | 0.00 | |
| 6538.00 | 6.00 | 0.37 | 1.25 | 0.00 | |
| 6539.00 | 7.00 | 0.43 | 1.66 | 0.00 | |
| 6540.00 | 8.00 | 0.48 | 2.11 | 0.00 | |
| 6541.00 | 9.00 | 0.55 | 2.63 | 0.00 | Stage of SW#1 |
| 6541.70 | 9.70 | 0.60 | 3.04 | 10.90 | |
| 6541.80 | 9.80 | 0.61 | 3.10 | 14.42 | |
| 6541.90 | 9.90 | 0.62 | 3.16 | 18.33 | |
| 6542.00 | 10.00 | 0.62 | 3.22 | 22.63 | |
| 6542.50 | 10.50 | 0.66 | 3.54 | 52.82 | |
| 6542.59 | 10.59 | 0.67 | 3.60 | 59.70 | Peak Stage |
| 6543.00 | 11.00 | 0.70 | 3.88 | 92.64 | |
| 6543.50 | 11.50 | 0.74 | 4.25 | 141.13 | |
| 6544.00 | 12.00 | 0.78 | 4.63 | 207.48 | |

J1, B2, S1
J27-RB

Drainage Area from J1, B2, S1, SWS(s)1: 10.8 acres
Total Contributing Drainage Area: 10.8 acres

SW#1: Emergency Spillway

| Elev | Stage (ft) | Area (ac) | Capacity (ac-ft) | Discharge (cfs) | |
|---------|---------------|--------------|---------------------|--------------------|--|
| 6554.50 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 6555.50 | 1.00 | 0.04 | 0.01 | 0.00 | |
| 6556.50 | 2.00 | 0.10 | 0.08 | 0.00 | |

| | | | | |
|---------|-------|------|------|--------|
| 6557.50 | 3.00 | 0.15 | 0.21 | 0.00 |
| 6558.50 | 4.00 | 0.20 | 0.39 | 0.00 |
| 6559.50 | 5.00 | 0.25 | 0.61 | 0.00 |
| 6560.50 | 6.00 | 0.30 | 0.89 | 0.00 |
| 6561.50 | 7.00 | 0.34 | 1.21 | 0.00 |
| 6562.00 | 7.50 | 0.37 | 1.39 | 0.00 |
| 6562.50 | 8.00 | 0.41 | 1.58 | 7.79 |
| 6562.66 | 8.16 | 0.43 | 1.65 | 10.35 |
| 6562.70 | 8.20 | 0.43 | 1.67 | 10.90 |
| 6562.80 | 8.30 | 0.44 | 1.71 | 14.42 |
| 6562.90 | 8.40 | 0.45 | 1.76 | 18.33 |
| 6563.00 | 8.50 | 0.46 | 1.80 | 22.63 |
| 6563.50 | 9.00 | 0.51 | 2.05 | 52.82 |
| 6564.00 | 9.50 | 0.58 | 2.32 | 92.64 |
| 6564.50 | 10.00 | 0.64 | 2.62 | 141.13 |
| 6565.00 | 10.50 | 0.71 | 2.96 | 207.48 |

Stage of SW#1

Peak Stage

J2, B1, S1
J27-RC

| | |
|---|-------------|
| Drainage Area from J2, B1, S1, SWS(s)1: | 14.8 acres |
| Total Contributing Drainage Area: | 143.4 acres |

SW#1: Emergency Spillway

| Elev | Stage (ft) | Area (ac) | Capacity (ac-ft) | Discharge (cfs) |
|------|---------------|--------------|---------------------|--------------------|
|------|---------------|--------------|---------------------|--------------------|

| | | | | |
|---------|------|------|------|--------|
| 6460.80 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6461.80 | 1.00 | 0.17 | 0.06 | 0.00 |
| 6462.80 | 2.00 | 0.27 | 0.28 | 0.00 |
| 6463.80 | 3.00 | 0.34 | 0.58 | 0.00 |
| 6464.80 | 4.00 | 0.43 | 0.97 | 0.00 |
| 6465.80 | 5.00 | 0.52 | 1.44 | 0.00 |
| 6466.80 | 6.00 | 0.63 | 2.02 | 0.00 |
| 6467.00 | 6.20 | 0.66 | 2.15 | 0.00 |
| 6467.70 | 6.90 | 0.74 | 2.63 | 20.85 |
| 6467.80 | 7.00 | 0.75 | 2.71 | 27.35 |
| 6467.90 | 7.10 | 0.76 | 2.78 | 34.50 |
| 6468.00 | 7.20 | 0.77 | 2.86 | 42.27 |
| 6468.50 | 7.70 | 0.83 | 3.26 | 94.82 |
| 6468.80 | 8.00 | 0.86 | 3.52 | 132.58 |
| 6468.99 | 8.19 | 0.89 | 3.68 | 158.90 |
| 6469.00 | 8.20 | 0.89 | 3.69 | 160.74 |
| 6469.50 | 8.70 | 0.95 | 4.15 | 237.78 |
| 6469.80 | 9.00 | 0.98 | 4.44 | 296.72 |
| 6470.00 | 9.20 | 1.00 | 4.64 | 339.41 |

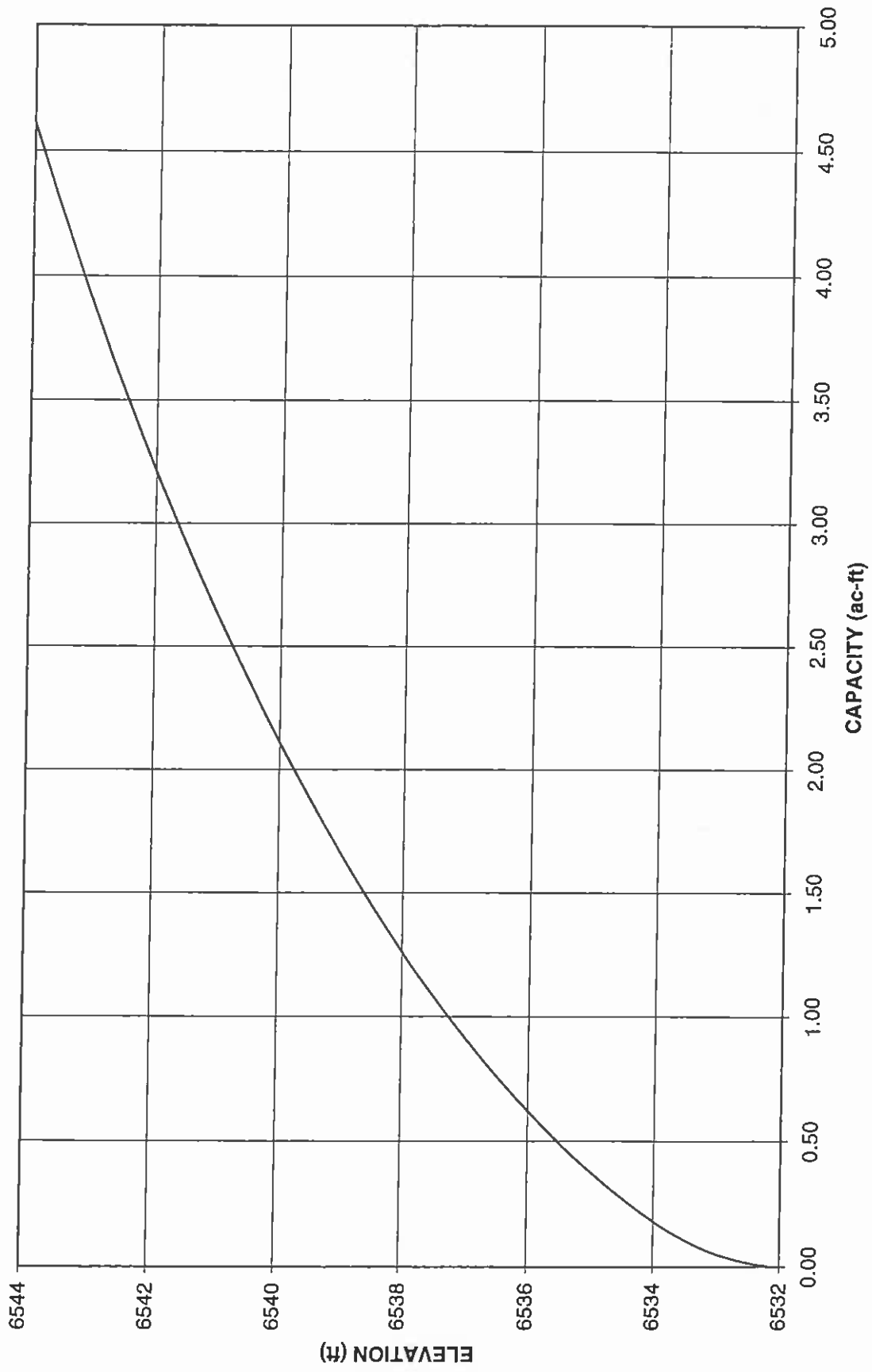
Stage of SW#1

Peak Stage

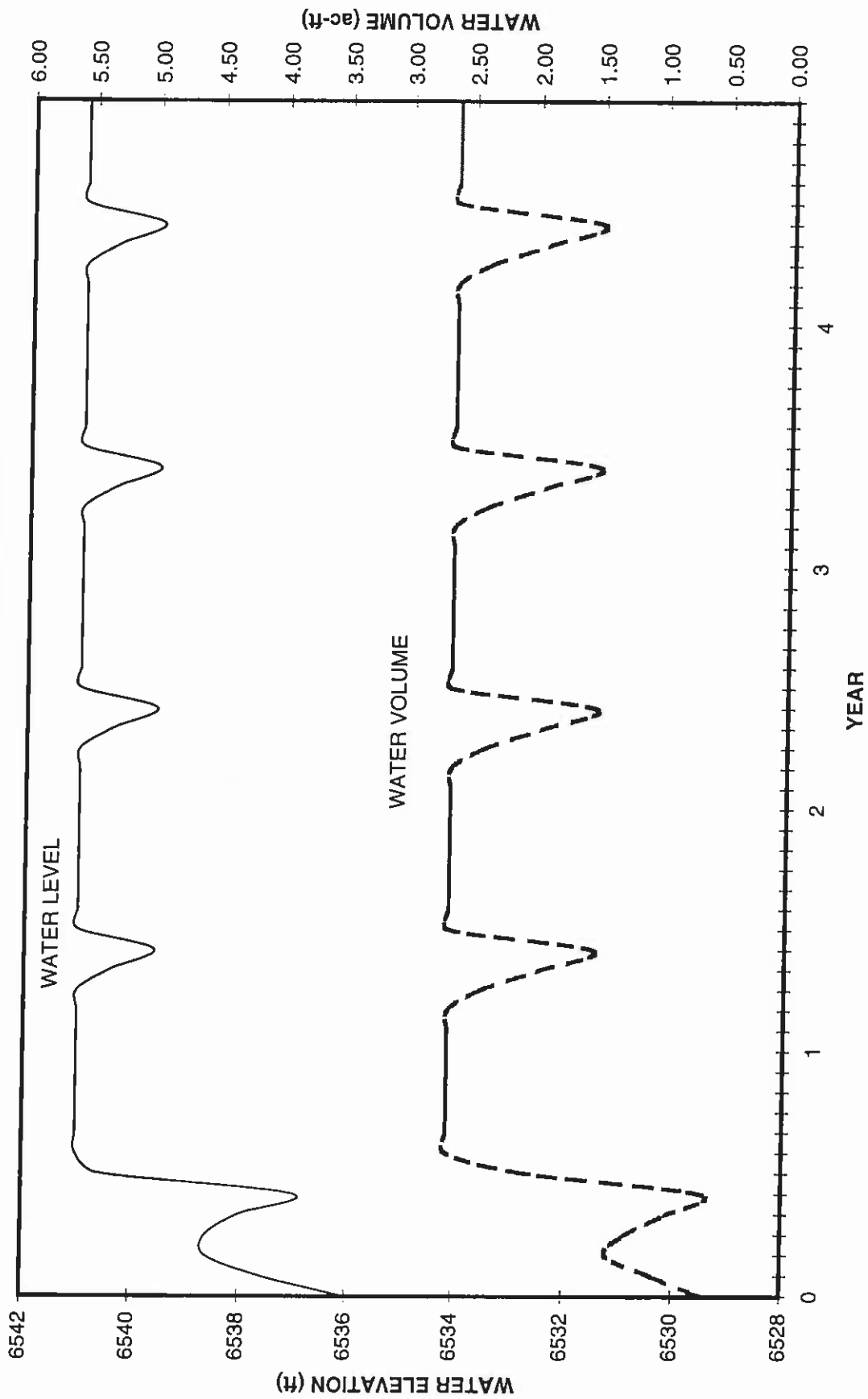
APPENDIX C

Water Persistence Calculations

PERMANENT IMPOUNDMENTJ27-RA
ELEVATION /CAPACITY CURVE



J27-RA PERMANENT IMPOUNDMENT
WATER PERSISTENCE EVALUATION



PEABODY WESTERN COAL COMPANY
PERMANENT IMPOUNDMENT POND WATER PERSISTENCE EVALUATION

| | January | February | March | April | May | June | July | August | September | October | November | December | End of Year 2 | End of Year 3 | End of Year 4 | End of Year 5 |
|----------------------------------|---------|----------|--------|--------|-------|-------|--------|--------|-----------|---------|----------|----------|---------------|---------------|---------------|---------------|
| Average Precipitation (inch) | 0.95 | 0.86 | 0.89 | 0.58 | 0.45 | 0.48 | 1.49 | 1.49 | 0.95 | 1.09 | 0.98 | 1.08 | 1.08 | 1.08 | 1.08 | 1.08 |
| Area (acres) | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 | 45.8 |
| Curve Number S | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| Run-Off (inches) | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| Run-Off (ac-ft) | 0.17 | 0.13 | 0.15 | 0.03 | 0.01 | 0.01 | 0.49 | 0.49 | 0.17 | 0.24 | 0.19 | 0.24 | 0.24 | 0.24 | 0.24 | 0.24 |
| Starting Pond Volume (ac-ft) | 0.66 | 0.50 | 0.55 | 0.13 | 0.03 | 0.04 | 1.85 | 1.85 | 0.68 | 0.93 | 0.72 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Pond Volume + Runoff (ac-ft) | 0 | 0.62 | 1.02 | 1.38 | 1.23 | 0.90 | 0.63 | 2.00 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 |
| Water Elevation (ft) | 0.66 | 1.12 | 1.57 | 1.51 | 1.26 | 0.94 | 2.48 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 |
| Water Surface Area (acres) | 6536 | 6537.6 | 6538.6 | 6538.6 | 6538 | 6537 | 6540.6 | 6541 | 6541 | 6541 | 6541 | 6541 | 6541 | 6541 | 6541 | 6541 |
| Evaporation Rate (inches/month) | 0.27 | 0.35 | 0.40 | 0.40 | 0.37 | 0.32 | 0.32 | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 |
| Evaporation (ac-ft) | 0.87 | 2.63 | 4.68 | 7.38 | 10.54 | 10.77 | 9.95 | 8.49 | 7.08 | 4.68 | 2.82 | 1.46 | 1.46 | 1.46 | 1.46 | 1.46 |
| Infiltration Rate (inches/month) | 0.02 | 0.08 | 0.16 | 0.25 | 0.32 | 0.29 | 0.43 | 0.39 | 0.32 | 0.21 | 0.13 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| Infiltration (ac-ft) | 1.054 | 0.952 | 1.054 | 1.02 | 1.054 | 1.02 | 1.054 | 1.054 | 1.02 | 1.054 | 1.02 | 1.054 | 1.054 | 1.054 | 1.054 | 1.054 |
| Total Water Loss (ac-ft) | 0.04 | 0.10 | 0.19 | 0.28 | 0.36 | 0.31 | 0.48 | 0.44 | 0.37 | 0.28 | 0.18 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| Total Water Change (ac-ft) | 0.62 | 0.40 | 0.36 | -0.15 | -0.32 | -0.28 | 1.37 | 1.42 | 0.28 | 0.67 | 0.54 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |
| Ending Pond Volume | 0.62 | 1.02 | 1.38 | 1.23 | 0.90 | 0.63 | 2.00 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 |
| Volume through Spillway | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.79 | 0.29 | 0.67 | 0.54 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |

Notes:

1) Run-off volumes based on SCS Runoff Curve Number method: $Q = (P-0.2S)^{0.5} / (P+0.8S)$

P = Accumulative Precipitation

S = $(1000/CN) - 10$

2) Evaporation and Infiltration rates based on data presented in the report entitled "Hydrologic and Engineering Studies at the Peabody Coal Company Mines" in Permit AZ-00013 Volume 27.

3) Maximum Pond Volume 2.63 ac-ft

Need Map