DESIGN REPORT

Sedimentation Structure

J3-G

Black Mesa Mine

Navajo County, Arizona

for

PEABODY COAL COMPANY



# TABLE OF CONTENTS

																														Page
INTR	ODUCTI	ON .				•	•	. •	•	•	•	•	•	•	•	•	•	•	•	•	•		•	•	•	•		•		1
INSP	ECTION	·	•	•		•	•	•	•	•	•		•	•		•		•	•	•		•	•	•	•	•	•	•	•	1
SITE	DESCR	IPT]	ои	•	•	•		•	•	•	•	•	•	•	•	•	•	•	•	•	•			•	•	•	•	•	•	2
	LAND	USE	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•		•	•	•	•	2
	EMBAN	KMEN	T	•	•	•	•	•	•	•	•		•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•		2
DESI	GN ANA	LYSE	S	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•		•	•	•	•	•	•	•	2
	GENER	AL .	•	•	•	•	•		•	•	•		•	•	•	•	•	•	•	•	•	•	•	•	•	•	•		•	2
	STABI	LITY		•	•	•	•	•		•	•	•	•	•	•	•	•	•		•	•	•	•	•	•	•	•	•	•	3
	HYDRO	LOGY		•	•	•	•			•	•	•	•	•	•	•	•	•	•		•	•	•	•	•	•	•	•	•	3
	HYDRA	ULIC	S	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	3
	S	p111	way	r a	ınd	C	ut	:f1	OW	7 (	The	ınr	el	•		•	•	•	•	•	•	•	•	•	•					5
	STORA	GE C	APA	CI	TY		•	•	•	•	•		•	•	•	•		•	•	•	•		•	•	•	•	•	•		5
A DDE1	TOTY A	_ 0	מחס	ΩŢ	00	v	ΑK	m	שע	יחד	A T	TT T		CA	τ (	דדו	ΑT	ידר	NIC	,										

#### INTRODUCTION

Sedimentation Structure J3-G will be an internal impoundment, designed and constructed by Peabody Coal Company as a temporary sedimentation structure to control runoff and sediment from the proposed mine airport at the Black Mesa Mine. The location of Structure J3-G is shown on Plate 1, Site Plan.

This design report contains information specific to Structure J3-G. Regional site information is presented in the "General Report, Kayenta and Black Mesa Mines, Navajo County, Arizona for Peabody Coal Company," along with the methods and results of analyses used for slope stability, hydrology and hydraulics.

#### INSPECTION

The proposed site of Structure J3-G was inspected by a senior geotechnical engineer from Dames & Moore in October, 1985 to ensure that the site is suitable and no adverse conditions exist to prevent the successful construction of the structure. A detailed geotechnical investigation was not performed.

#### SITE DESCRIPTION

#### LAND USE

Structure J3-G has a 241.8-acre tributary drainage area and is located near Coal Mine Wash at the Black Mesa Mine. The watershed is classified as 86% reclaimed and 14% disturbed.

#### **EMBANKMENT**

The structure will not have an embankment.

#### DESIGN ANALYSES

#### **GENERAL**

Structure J3-G was designed by an interdisciplinary team of engineers from Dames & Moore. The design was performed in accordance with applicable 30 CFR 780 and 816 regulations of the United States Department of Interior, Office of Surface Mining (OSM) and included a review of available project files. The most current information contained in the Peabody Coal Company files includes topographic maps developed from aerial photography flown in 1985 for Peabody Coal Company and was used in the analyses of the structure.

#### STABILITY

A stability analysis does not need to be performed for this structure.

#### HYDROLOGY

The hydrologic analysis was completed using the U.S. Army Corps of Engineers generalized computer program HEC-1, Flood Hydrograph Package. Structure J3-G does not have a spillway. Therefore, it was designed to contain the runoff from the Probable Maximum Precipitation (PMP).

The following parameters were used in the hydrologic analysis:

2. 3. 4. 5.	Water Course length, L	
	Probable Maximum Precipitation	
	Local Storm (6 hour) 8.8 in	ì •
	General Storm (72 hour - August) 11.1 in	1.
	General Storm (6 hour - Augsut) 4.7 in	1.
7.	Drainage Area 241.8 ac	res

## HYDRAULICS

The HEC-1 program was used to evaluate inflow to the planned sedimentation structure and the resulting water surface elevations. The initial conditions and results of the analysis are summarized in the following table.

J3-G HYDRAULICS

Units	General Storm PMP	Local Storm PMP
Initial Reservoir Volume		
Condition	Empty	Empty
Inflow		
Peak Flow cfs	179	2052
Volume acre-ft	193.8	144.3
Storage		
Maximum Allowable		
Water Surface	6E10 00	6E10 00
Elevation ft	6510.00	6510.00
Peak Stage ft	6504.42	6501.90
Peak Storage acre-ft	193.8	144.3
Storage Capacity acre-ft	308.9	308.9

### Spillway and Outflow Channel

Structure J3-G will not have a spillway or outflow channel because it is designed to contain all runoff from the PMP.

#### STORAGE CAPACITY

The impoundment volume-elevation curve shown on Plate 2, Volume-Elevation Curve, J3-G is based on site specific topographic data developed for Peabody Coal Company in 1985, and 1985 site specific surveys, where available.

The calculations for the sediment load entering Structure J3-G were made utilizing the Universal Soil Loss Equation with the following parameters:

- 1. Rainfall Factor, R . . . . . . . . . . . . 40
- Soil Erodibility Factor, K . . . . . . 0.42
- 3. Slope Factor, LS . . . . . . . . . . . 3.37
- 4. Cover Factor, C . . . . . . . . . 0.269
- 5. Erosion Control Factor, P . . . . . . 1.0

The hydrologic analysis gives the storage volume required to contain the 10-year, 24-hour storm, and the remaining storage volume available for storing sediment. The storage capacity of J3-G is shown on Plate 2, Volume-Elevation Curve, J3-G, and the results of the sediment inflow analysis are summarized in the following table.

# J3-G STORAGE

	General PMP	Local PMP
Total Storage Capacity	308.9	308.9 acre-ft
Storm Inflow	193.8	144.3 acre-ft
Available Sediment Storage Capacity		
Sediment Inflow Rate	1.71	1.71 acre-ft/yr
Sediment Storage Life	67	96 vrs

\* \* \*

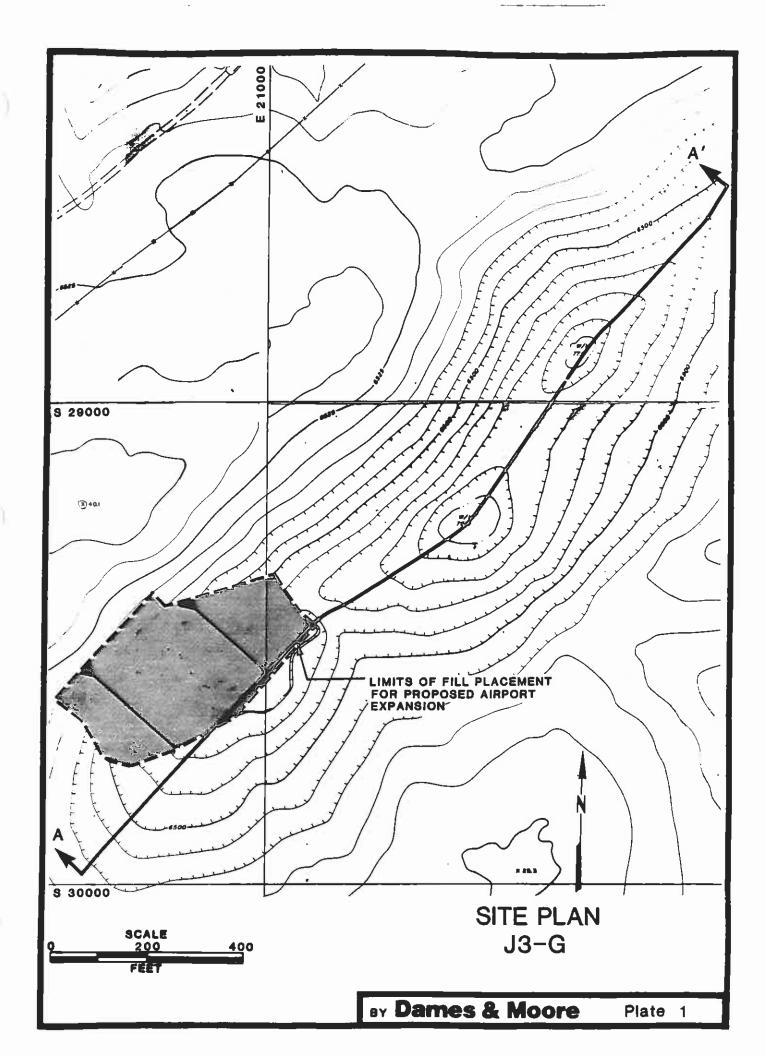
The following plates and appendix are attached and complete this design report.

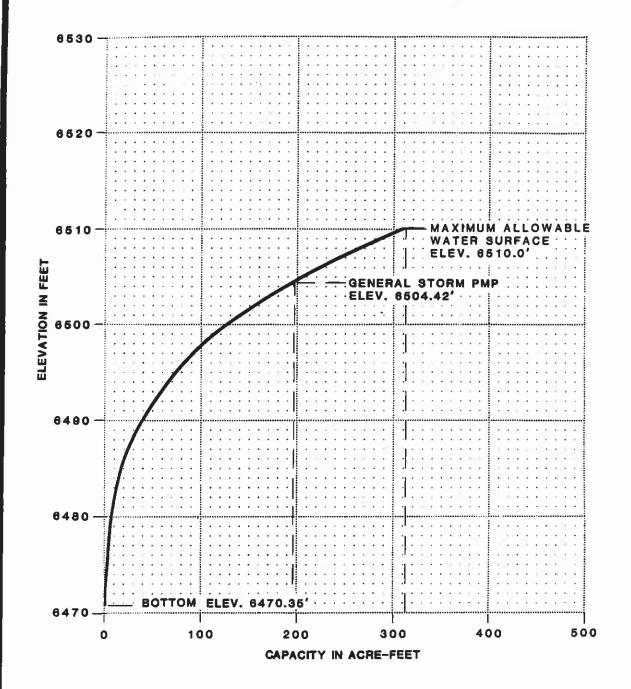
Plate I - Site Plan J3-G

Plate 2 - Volume-Elevation Curve J3-G

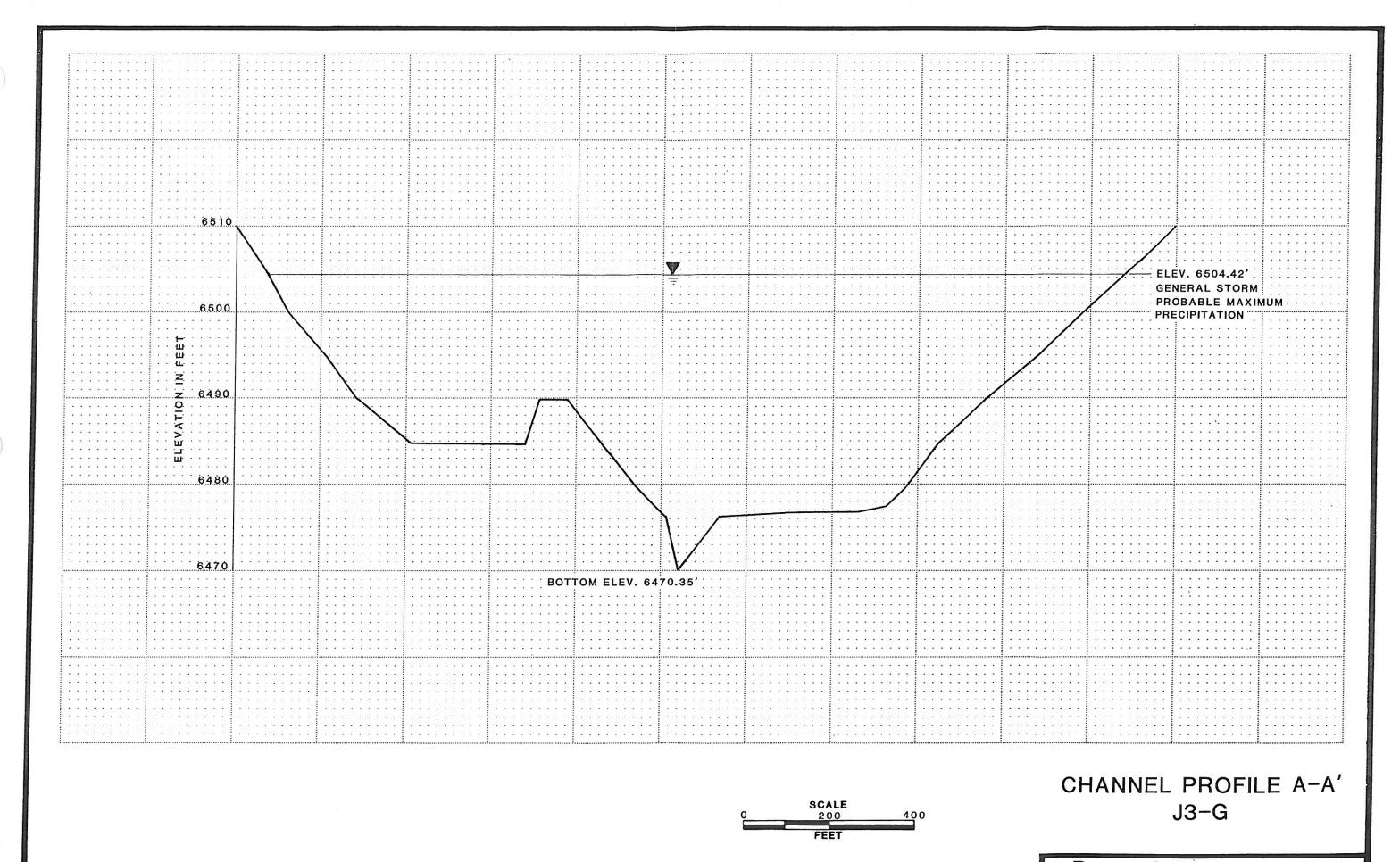
Plate 3 - Channel Profile J3-G, A-A'

Appendix A - Hydrology and Hydraulic Calculations





VOLUME-ELEVATION CURVE J3-G



# APPENDIX A HYDROLOGY AND HYDRAULIC CALCULATIONS

\_T0 E0 \_\_\_\_ DATE REVISIONS

TIME OF CONCENTIZATION

ELEVATION DIFFERENCE = 83

WATER COURSE LEDOUTH = 6770' = 1,28 mi

Te =0,630 hr

LAG TIME = 0.6Te = 0.63 hr

SCS CUEUF NUMBER

DRAINAGE	COVER	HydroLock	Soil	MEIGHTED
ARFA (ac)	TYPE	CONDITION	TYPE	CURUE NUMBER
207.4	reclaimed			87 (.86)
34.4	reclaimed (pre-law) distributed Convey)		C	92 (.14)
•	( hamed			87.7

use 88

CHECKED BY BANY "

)

DEAINAGE BASIN AREA

0.378 SO MILE 241.8 ACRE

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CHECKED BY BAM

# UNIVERSAL Soil Loss EQUATION

RAINPALL FACTOR

R= 40

SOIL ERODIBILITY FACTOR

SOIL TYPE = 100 % EX #35

K=0.42

SLOPE FACTOR

LEDGTH(II)	DELEV (fi)	SLOPE (%	) LS
800	105	13.1	5.924.68 (4)
600	40	6.7	1.91 453 (.3)
700	35	5,	142115 (,3)
			267334

COVER FACTOR

P=1.0

SEDIMENT INFLOW

A = 40(.42)(3.37)(.269)(1.0) = 15.23 ton/acre/year

A = 15.23( $\frac{1}{2047}$ )(241.8)(A) = 1.62 acre-feet/year

Dames & Moore

in

SUBJECT 33-G COMPRISON SHEET OF

REVISIONS
BY \_\_\_\_\_\_ DATE \_\_\_\_\_TO E0 \_\_\_\_
BY \_\_\_\_\_ DATE \_\_\_\_\_TO E0 \_\_\_\_

CHECKED BY

Fras.	Jos.	for Sung date bother = 6470.35
6472.02	04	
6480	5.07	No Spills my
LA85	14,84	No cetst
6440	36.6	140 02031
6495	71.0	
6500	126.1	
6505	202.6	
6510	3089	
6515	443.8	